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RELAXATION AT CRITICAL POINTS: DETERMINISTIC AND STOCHASTIC THE--ETC(U)

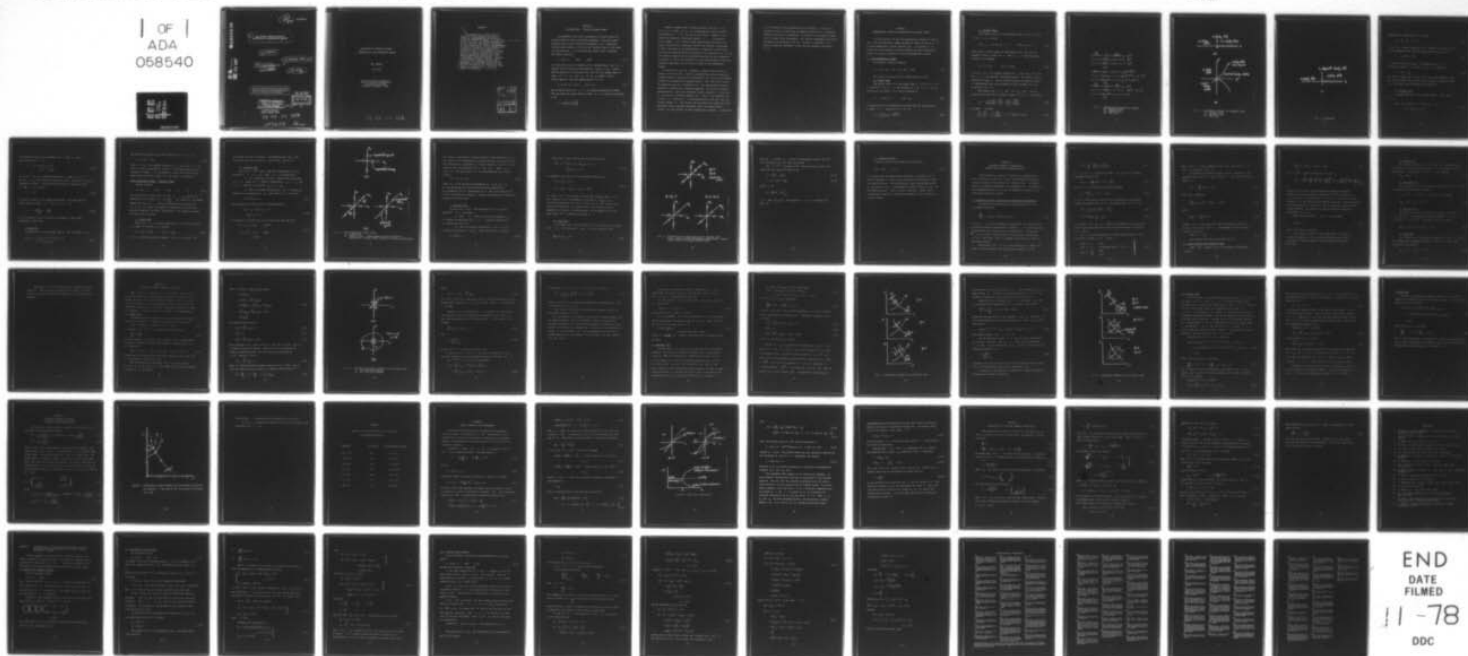
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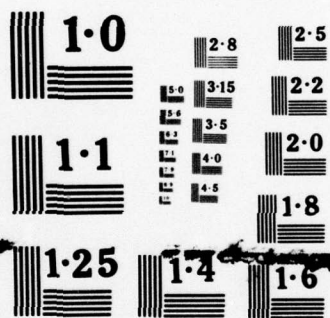
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6 RELAXATION AT CRITICAL POINTS:
DETERMINISTIC AND STOCHASTIC THEORY.

10 Marc Mangel

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RELAXATION AT CRITICAL POINTS:
DETERMINISTIC AND STOCHASTIC THEORY

Marc Mangel

June 1978

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ABSTRACT

A generalized critical point is characterized by totally non-linear dynamics. ~~We formulate~~ the deterministic and stochastic theory of relaxation *is formulated* at such a point. Canonical problems are used to motivate the general solutions. In the deterministic theory, ~~we show that~~ at the critical point certain modes have polynomial (rather than exponential) growth or decay. The stochastic relaxation rates can be calculated in terms of various incomplete special functions. Three examples are considered. First, a substrate inhibited reaction (marginal type dynamical system). Second, the relaxation of a mean field ferromagnet. ~~We obtain a result that generalizes the~~ work of Griffiths et al. Third, ~~we con-~~ sider the relaxation of a critical harmonic oscillator, *is considered*.

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SECTION 1

INTRODUCTION: "CRITICAL SLOWING DOWN"

Thermodynamic and kinetic generalized critical points are characterized by totally non-linear dynamics. Such non-linear dynamics lead to many interesting phenomena, e.g., "anomalous" fluctuations (treated in (1)) and the "slowing" down of the decay of a perturbation. To illustrate the latter effect, consider the kinetic equation:

$$\dot{x} = b(x, \alpha) \quad x \in \mathbb{R}^1 \quad \alpha \in \mathbb{R}^j \quad (1.1)$$

for which the origin is assumed to be a steady state: $b(0, \alpha) = 0$. Suppose that the system is perturbed to a value $x = x_0$. A well defined problem is to calculate the time that the system takes to reach δ ($0 < \delta \ll x_0$) from x_0 . If x_0 is "small," then a natural approach involves approximating (1.1) by

$$\dot{x} = b'(0, \alpha)x + o(x^2) \quad x(0) = x_0. \quad (1.2)$$

Now we assume that $b'(0, \alpha) < 0$, so that the perturbation decays. The time that the system takes to reach $x = \delta$ is easily calculated to be

$$t_\delta = \frac{1}{b'(0, \alpha)} \ln \left[\frac{\delta}{x_0} \right] \quad (1.3)$$

However, suppose that for some critical value of $\alpha = \alpha_c$, $b'(0, \alpha_c) = 0$. Then $(0, \alpha_c)$ is a "generalized critical" point: the dynamics at $\alpha = \alpha_c$ are totally non-linear. Equation (1.3) yields the physically ridiculous result $t_\delta = \infty$. Furthermore, (1.2) becomes $\dot{x} = 0$. Both of these difficulties are due to improper linearization procedures, and not any physical divergences. In fact, the decay of the perturbation is algebraic in time, with the exact form determined by the nature of the singularity at $(0, \alpha_c)$. Such simple problems and the canonical bifurcations are considered in section 2. The points essential to the understanding of critical relaxation phenomena can be gained by study of one-dimensional systems.

If fluctuations are not included, a steady state can not be attained in finite time. Since the deterministic forces vanish as a steady state or equilibrium is approached, the ratio of fluctuation intensity to deterministic dynamics grows. Thus, the proper theory of relaxation must be a stochastic one. The deterministic kinetic equation is modified by a Langevin approach. We use the diffusion approximation to treat the stochastic kinetic equation. In particular, we derive a diffusion equation for $T(x'|x)$, the expected time to reach x' , starting at x and conditioned on the fact that the process reaches x' . We analyze the one-dimensional equations fully and obtain certain special functions, which are generalized in section 4 to the solution of multi-dimensional problems. In sections

5-7, we consider three applications of the theory. In section 5, relaxation from a steady state of marginal stability in a substrate inhibited reaction is considered. In section 6, we consider relaxation of a mean field ferromagnet. Our results complement and extend the results of Griffiths et al (2). Finally, in section 7, we discuss relaxation phenomena in the critical harmonic oscillator (1, 3).

SECTION 2

DETERMINISTIC THEORY OF RELAXATION AT CRITICAL POINTS

In this section, we give the deterministic theory of relaxation. Our classification scheme extends the ideas of Kubo et al (4) to multi-dimensional systems (section 2.2). In section 2.1, we stress the one-dimensional results, because the multi-dimensional theory is a natural extension of the one-dimensional results.

2.1 ONE-DIMENSIONAL SYSTEMS

We consider a kinetic equation

$$\dot{x} = b(x, \alpha_c) \quad x(0) = x_0 \quad x \in \mathbb{R}^1 \quad \alpha \in \mathbb{R}^n. \quad (2.1)$$

The origin is assumed to be a steady state of (2.1).

A. Normal Type

The steady state is of the normal type if $b'(0, \alpha) \neq 0$. It is stable if $b'(0, \alpha) < 0$ and unstable if $b'(0, \alpha) > 0$. In the vicinity of the origin, (2.1) can be replaced by

$$\dot{x} = b'(0, \alpha) x \quad x(0) = x_0 \quad (2.2)$$

As mentioned in the introduction, the time that the system takes to reach $x = \delta$, starting at $x = x_0$ is

$$t_\delta = \frac{1}{|b'(0, \alpha)|} \ln \left[\frac{x_0}{\delta} \right]. \quad (2.3)$$

B. Marginal Type

The steady state is of the marginal type if $\alpha \in \mathbb{R}^1$ and for a value $\alpha = \alpha_c$ we have

$$b(0, \alpha_c) = b'(0, \alpha_c) = 0, \quad b''(0, \alpha_c) \neq 0 \quad (2.4)$$

There exists a local change of coordinates (e.g., (5), (6), or Appendix A here) so that for α near α_c , x near the origin equation (2.1) becomes

$$\dot{y} = y^2 - \beta(\alpha), \quad y(0) = y_0(x_0) \quad (2.5)$$

In (2.5), $\beta(\alpha)$ is a regular function of α and $\beta(\alpha_c) = 0$. We call $\alpha = \alpha_c$ the marginal bifurcation point. The flow of (2.5) is sketched in figure 1. The bifurcation picture is shown in figure 2. The marginal case was considered briefly by Kubo et al (4) and Nitzan et al (7).

Now suppose that $\beta > 0$ and $-\sqrt{\beta} < y_0 < \sqrt{\beta}$. One can calculate the time that it takes to reach $y_1 = -\sqrt{\beta} + \delta$. We obtain

$$t_{y_1} = \frac{1}{2\sqrt{\beta}} \left\{ \ln \left\{ \frac{y_1 - \sqrt{\beta}}{y_1 + \sqrt{\beta}} \right\} - \ln \left\{ \frac{y_0 - \sqrt{\beta}}{y_0 + \sqrt{\beta}} \right\} \right\} \quad (2.6)$$

For small δ we have

$$\frac{y_1 - \sqrt{\beta}}{y_1 + \sqrt{\beta}} = \frac{1 - \sqrt{\beta}/y_1}{1 + \sqrt{\beta}/y_1} = (1 - \sqrt{\beta}/y_1)^2 + o(\beta) \quad (2.7)$$

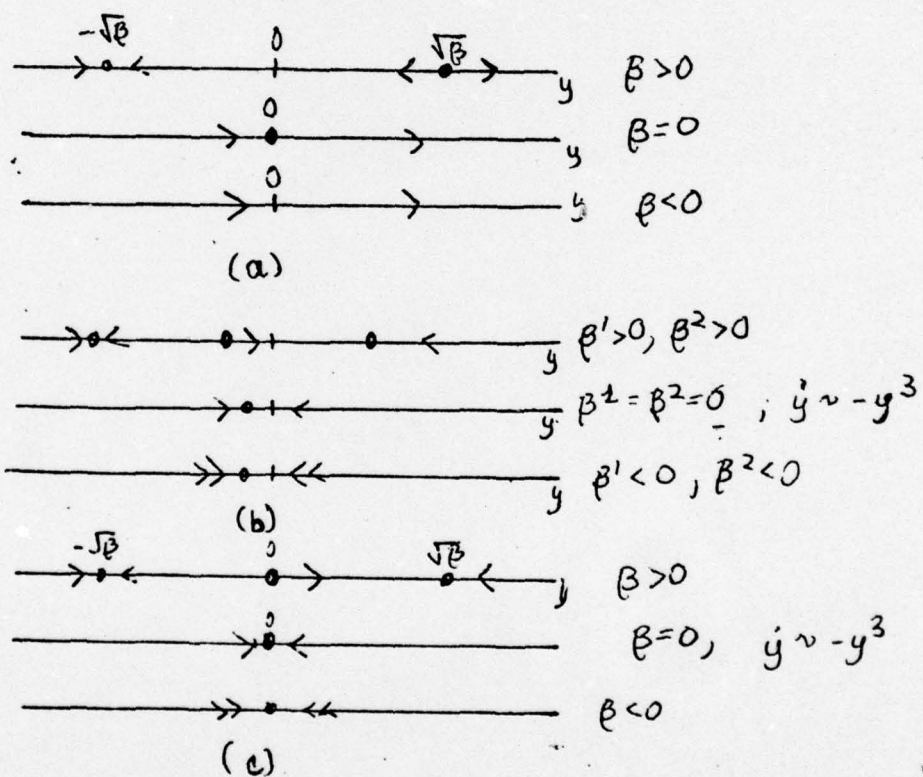
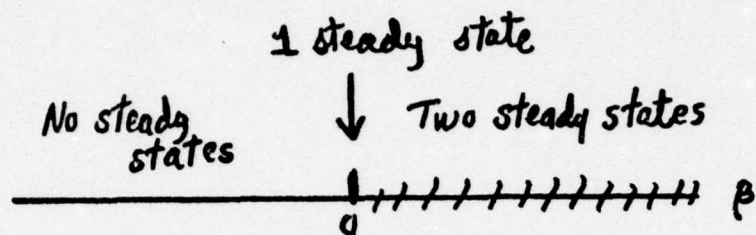
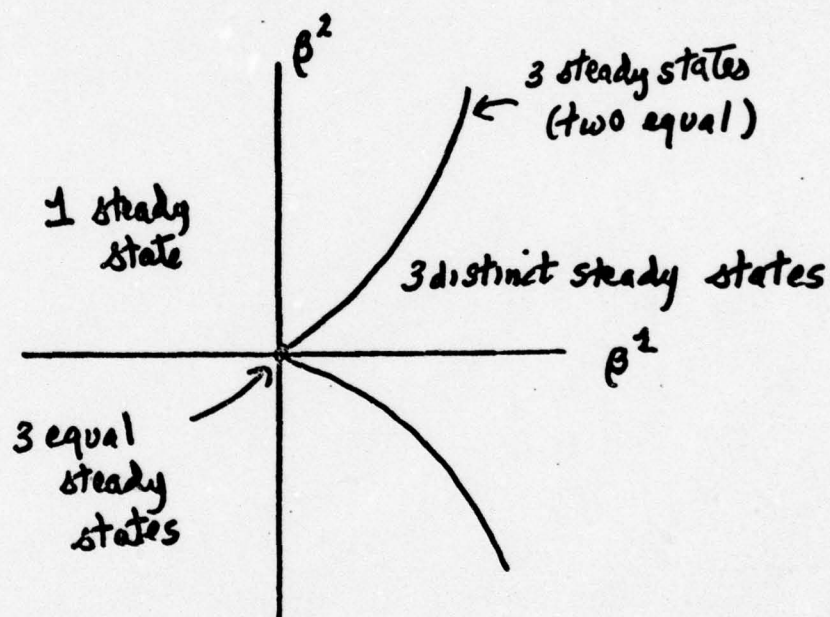


FIG. 1: DYNAMICS OF THE CANONICAL SYSTEMS
 (a) MARGINAL TYPE
 (b) CRITICAL TYPE
 (c) HOPF TYPE

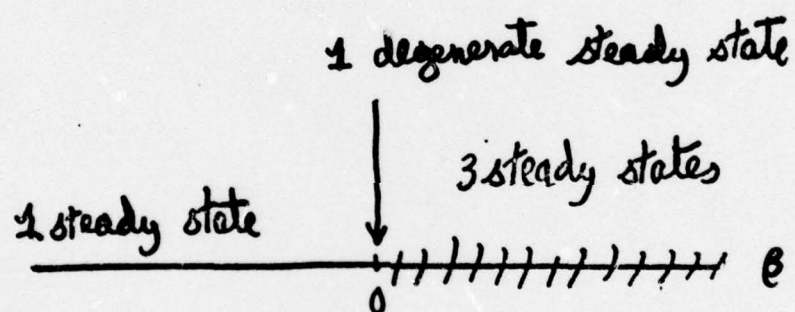


(a)



(b)

FIG. 2: BIFURCATION PICTURES IN PARAMETER SPACE
 (a) MARGINAL TYPE;
 (b) CRITICAL TYPE;
 (c) HOPF TYPE



(c)

FIG. 2: (Continued)

Expanding the logarithms in (2.6) gives

$$t_{y_1} \sim \frac{1}{y_0} - \frac{1}{y_1} + o(\beta) \quad (2.8)$$

so that t_{y_1} remains finite as $\beta \rightarrow 0$. Clearly, this result would not be obtained had we used the linearized version of (2.5):

$$y' = -2\sqrt{\beta} (y + \sqrt{\beta}) \quad (2.9)$$

In another possible situation $\beta=0$. Suppose that $y_0 < 0$.

The time to reach $\delta < 0$ from y_0 ($y_0 < \delta$) is (exactly)

$$t = -\frac{1}{\delta} + \frac{1}{y_0} \quad (2.10)$$

The point of importance is that (2.8, 2.9) yield algebraic forms for the relaxation time, whereas (2.3) yields a logarithmic time (i.e., algebraic versus exponential relaxation).

C. Critical Type

A steady state is of the critical type if $\alpha \in R^2$ and for

$$\alpha = \alpha_c$$

$$b(0, \alpha_c) = b'(0, \alpha_c) = b''(0, \alpha_c) = 0 \quad (2.11)$$

$$b'''(0, \alpha_c) \neq 0$$

The canonical form of the dynamics, for α near α_c and y near 0 is (for $b''' < 0$)

$$\begin{aligned}\dot{y} &= -y^3 + \beta^1(\alpha)y + \beta^2(\alpha) \\ y(0) &= y_0(x_0)\end{aligned}\tag{2.12}$$

In (2.12), $\beta(\alpha)$ is a regular function of α and $\beta(\alpha_c) = 0$.

We call $\alpha = \alpha_c$ the critical bifurcation point. The flow of (2.12) is sketched in figure 1. The bifurcation picture is shown in figure

2. When $\alpha = \alpha_c$, we have

$$\dot{y} = -y^3\tag{2.13}$$

so that the origin is very weakly attracting. The time that the system takes to reach $y = \delta$ from $y = y_1 > \delta$ is

$$t_\delta = -\frac{1}{2} \left[\frac{1}{y_1^2} - \frac{1}{\delta^2} \right]\tag{2.14}$$

As in the marginal case, we obtain an algebraic, rather than exponential, decay rate.

D. Hopf Type

A steady state is of the Hopf type if $\alpha \in \mathbb{R}^1$ and when $\alpha = \alpha_c$

$$\begin{aligned}b(0, \alpha_c) &= b'(0, \alpha_c) = b''(0, \alpha_c) = 0 \\ b'''(0, \alpha_c) &\neq 0\end{aligned}\tag{2.15}$$

The canonical dynamics (8) in this case (for $b''' < 0$) are

$$\dot{y} = -y(y^2 - \beta(\alpha)) \quad (2.16)$$

where $\beta = \beta(\alpha)$ is a regular function of α and $\beta(\alpha_c) = 0$. The flow of (2.16) is sketched in figure 1. The bifurcation picture is sketched in figure 2. It is important to note the difference between Hopf and critical cases (i.e. the number of parameters).

MULTI-DIMENSIONAL THEORY: CANONICAL FORMS

We now consider

$$\dot{x} = b(x, \alpha) \quad x \in \mathbb{R}^n \quad \alpha \in \mathbb{R}^1 \quad \text{or} \quad \mathbb{R}^2 \quad (2.17)$$

with the origin a steady state. We let $\lambda_1, \dots, \lambda_n$ denote the eigenvalues of the matrix $B = (b^i_{,j}) \Big|_0$. For simplicity, we assume that there are n distinct eigenvalues and eigenvectors. Let k_+, k_-, k_0 denote the number of eigenvalues with real part positive, negative, and zero, respectively. The dynamical systems are classified as follows.

A. Normal Case

Hence $k_0 = 0$. It is well known that (2.17) can be replaced by a change of variables $x \rightarrow y$ so that

$$\dot{y}^i = \lambda_j y^i + o(y^2) \quad y^i(0) = y^i(x_0) \quad (2.18)$$

If $k_+ = 0$, then the origin is stable. If $k_+ > 0$, then \mathbb{R}^n can

be divided into two sub-spaces: an expanding part (W_e), and a contracting part (W_c) (figure 3), with $\dim W_e + \dim W_c = n$.

B. Marginal Case

We now let $\alpha \in \mathbb{R}^1$ vary. Then the eigenvalues of B are functions of α : $\lambda_k = \lambda_k(\alpha)$. When $\alpha = \alpha_c$ we assume that,

1) All eigenvalues are real. Exactly one eigenvalue $\lambda_0(\alpha_c) = 0$. There are k negative eigenvalues, $\lambda_1, \dots, \lambda_k$ and $n - 1 - k$ positive eigenvalues $\lambda_{k+1}, \dots, \lambda_{n-1}$.

2) There are enough eigenvectors. Let Z denote the eigenvector corresponding to λ_0 . Then from (2.17), we obtain,

$$\dot{Z} = \tilde{b}(y(Z), \alpha) \quad (2.19)$$

The marginal type steady state is characterized by

$$\begin{aligned} \tilde{b}(0, \alpha_c) &= \tilde{b}_Z(0, \alpha_c) = 0 \\ \tilde{b}_{ZZ}(0, \alpha_c) &\neq 0 \end{aligned} \quad (2.20)$$

In appendix A, we show that (2.17) can be put into the form

$$\begin{aligned} \dot{y}^i &= \lambda_i y^i + o(y^2) & y^i \in \mathbb{R}^{n-1} \\ \dot{y}^0 &= (y^0)^2 \pm \beta(\alpha) & y^0 \in \mathbb{R}^1 \\ &+ o(y^3) \end{aligned} \quad (2.21)$$

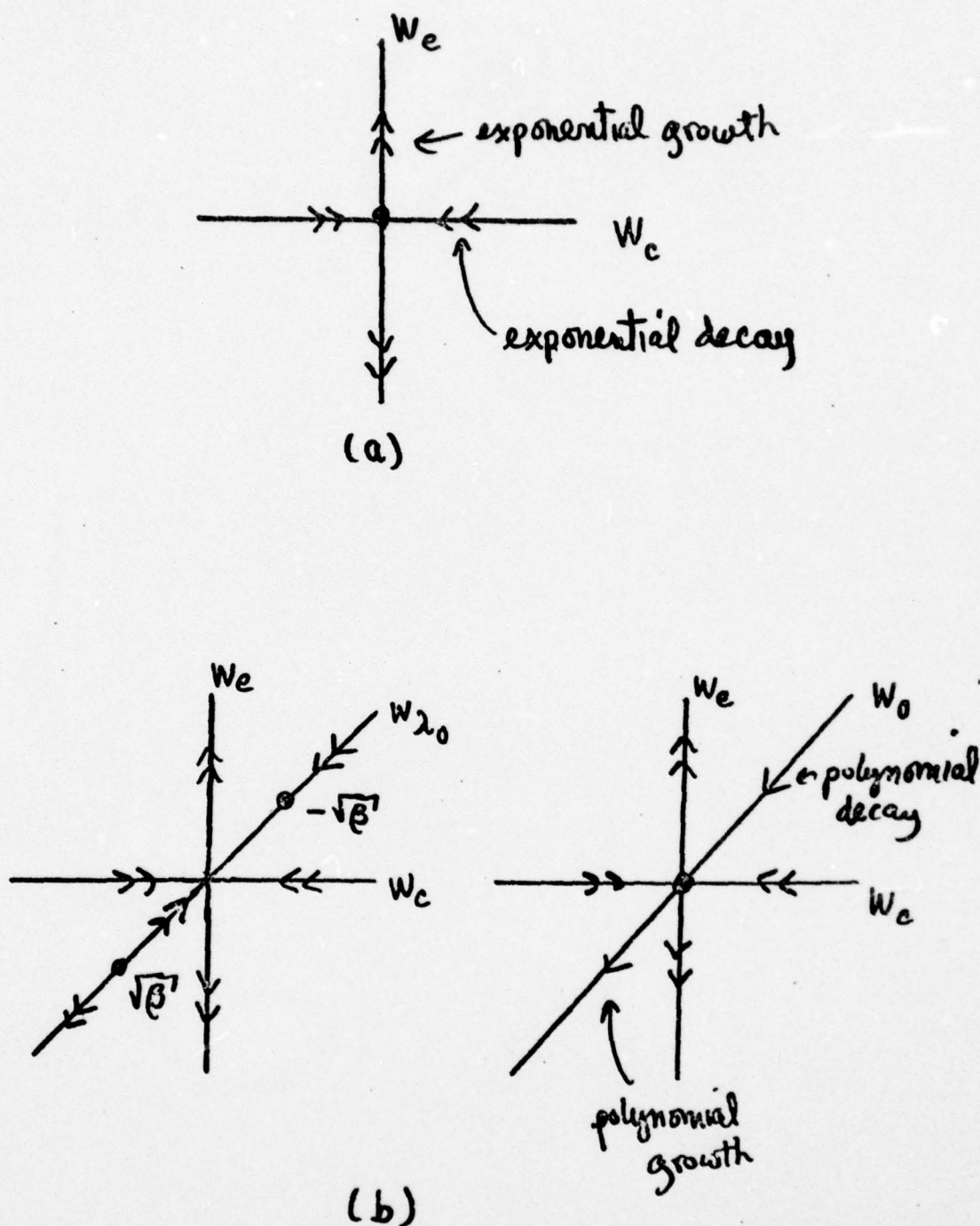


FIG. 3: MULTI-DIMENSIONAL PHASE SPACES.

- (a) NORMAL TYPE
- (b) MARGINAL TYPE: DOUBLE ARROWS INDICATE EXPONENTIAL GROWTH/DECAY; SINGLE ARROWS INDICATE POLYNOMIAL GROWTH/DECAY

Our result is approximate, whereas Arnold (5) and Shoshaitshvili (6) show there exist transformations which eliminate the higher terms. The construction in appendix A is useful, however, in that it gives explicit ways of calculating the y and $\beta(\alpha)$. When $\alpha = \alpha_c$, $\beta(\alpha_c) = 0$. The phase space R^n is now decomposed into a direct product

$$R^n = W_0 + W_e + W_c \quad (2.22)$$

where W_0 is the manifold corresponding to λ_0 and W_e , W_c are the expanding and contracting sub-spaces respectively.

The assumption that all eigenvalues of B were real affected the form of the canonical equations. Complex eigenvalues are explicitly treated in the Hopf case.

C. Critical Type

In this case, $\alpha \in R^2$. The eigenvalues of B are still denoted by $\lambda(\alpha)$. We assume:

1) When $\alpha = \alpha_c$ there is one zero eigenvalue, λ_0 , k negative eigenvalues and $n - k - 1$ positive eigenvalues. All eigenvalues are real.

2) There are enough eigenvectors. Let Z be the eigenvector belonging to $\lambda_0(\alpha)$. Then from (2.17), we obtain

$$\dot{Z} = \tilde{b}(y(Z), \alpha) \quad (2.23)$$

The critical type steady state is characterized by

$$\begin{aligned}\tilde{b}(0, \alpha_c) = \tilde{b}_z(0, \alpha_c) = \tilde{b}_{zz}(0, \alpha_c) &= 0 \\ \tilde{b}_{zzz}(0, \alpha_c) &\neq 0\end{aligned}\tag{2.24}$$

In appendix A, we show that the canonical dynamics are

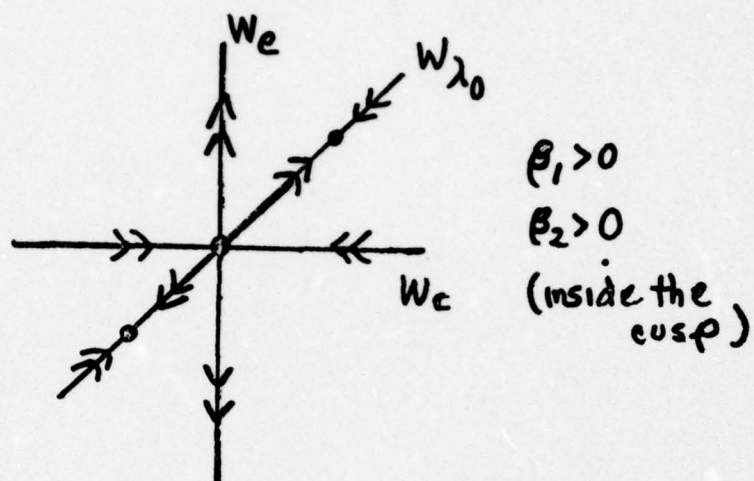
$$\begin{aligned}\dot{y}^i &= \lambda_i y^i + o(y^2) \\ \dot{z} &= \pm(z^3) - \beta_1(\alpha)z - \beta_2(\alpha) + o(z^4)\end{aligned}\tag{2.25}$$

In (2.25), $\beta(\alpha)$ is a regular function that vanishes when $\alpha = \alpha_c$. The \pm sign in (2.25) corresponds to the sign of $\tilde{b}_{zzz}(0, \alpha_c)$. Arnold and Shoshaitshvili state a theorem in which the higher order terms are eliminated. As remarked above, the constructions in appendix A are useful for applications. The decomposition of the phase space R^n is sketched in figure 4.

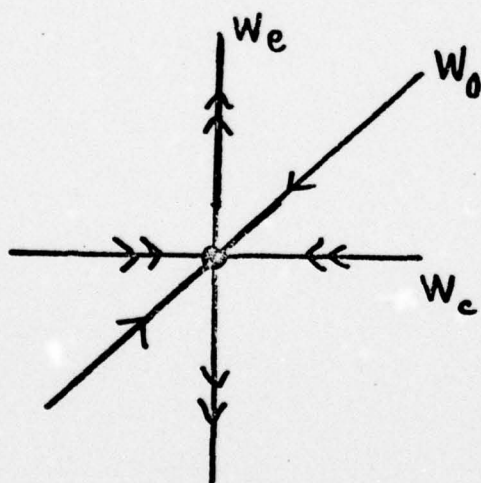
D. Hopf Type

In the Hopf case, $\alpha \in R^1$ and some of the eigenvalues are complex. When $\alpha = \alpha_c$ one eigenvalue, $\lambda_0(\alpha)$ is a pure imaginary with

$$\left. \frac{d}{d\alpha} \operatorname{Re} \lambda_0(\alpha) \right|_{\alpha_c} \neq 0\tag{2.26}$$



$$\beta_1 = \beta_2 = 0$$



$$\beta_1 < 0, \beta_2 < 0$$

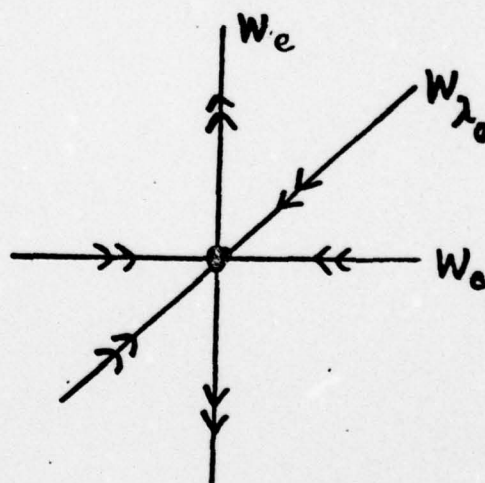


FIG. 4: DECOMPOSITION OF PHASE SPACE IN THE CRITICAL CASE. DOUBLE ARROWS INDICATE EXPONENTIAL GROWTH/DECAY. SINGLE ARROWS INDICATE POLYNOMIAL GROWTH/DECAY.

Thus, as α crosses α_c , a pair of eigenvalues crosses from the left half plane into the right half plane.

Let $x = re^{i\theta}$. Fenichel (1975) (also see Arnold (1972)) has shown that the canonical dynamics are

$$\dot{r} = \pm(b_1 r^3 - \eta \gamma_1 r) \quad (2.27)$$

$$\dot{\theta} = \lambda_2 + b_2 r^2 + \eta \gamma_1 r \quad (2.28)$$

where γ_1 is

$$\gamma_1 = \left. \frac{d}{d\alpha} \operatorname{Re} \lambda_+(\alpha) \right|_{\alpha_c},$$

$\lambda_2 > 0$ and $b_1, b_2 \neq 0$. The function $\eta = \eta(\alpha)$ is regular and $\eta(0) = 0$.

E. Relaxation Rates

Given an initial displacement from the origin

$$y(0) = \{y_0, \dots, y_{n-1}\} \quad (2.25)$$

it is clear that the appropriate relaxation (or growth) rate of the k^{th} component (or mode) can be explicitly calculated by using the canonical forms. The calculations reveal exponential growth in W_e , decay in W_c , and polynomial growth or decay in W_0 (at bifurcation points). Thus, we have a complete, albeit local, deterministic theory for relaxation phenomena in the vicinity of critical points.

SECTION 3

STOCHASTIC THEORY OF RELAXATION: FORMULATION AND ONE-DIMENSIONAL RESULTS

The deterministic theory of section 2 is approximate in that it ignores fluctuations. Since the deterministic dynamics vanish (to perhaps second order) at a steady state, the proper theory of relaxation phenomena is a stochastic one. Our theory is still phenomenological, but it may be possible to connect it to underlying statistical physics.

3.1 STOCHASTIC KINETIC EQUATION AND DIFFUSION APPROXIMATION

We replace the deterministic kinetic equation (2.17) by the Langevin equation:

$$\frac{d\tilde{x}_\tau^i}{dt} = b^i(\tilde{x}_\tau) + \frac{\sqrt{\epsilon}}{\tau} \sigma_j^i(x) \tilde{y}^j(t/\tau) \quad (3.1)$$

In (3.1), τ is a small parameter relating the time scales of the fluctuations and the deterministic dynamics, ϵ is a small parameter characterizing the intensity of the fluctuations. The process \tilde{y}^j is a zero mean, mixing process (for more exact assumptions, see (9)). The field $\sigma_j^i(x)$ is assumed to be known, or given by some prescription.

The process $\tilde{y}(S)$ in (3.1) has correlations. Hence, our model is more reasonable than "white noise" models. We let

$$\gamma^{kl} = \int_0^\infty E \left[\tilde{y}^k(s) \tilde{y}^l(0) \right] ds \quad (3.2)$$

As $\tau \rightarrow 0$, $x_\tau \rightarrow x$, a diffusion process. If $u_0(x)$ is a bounded, measurable function and

$$u(x, t) = E \left\{ u_0(\tilde{x}(t)) \mid \tilde{x}(0) = x \right\}, \quad (3.3)$$

then $u(x, t)$ satisfies the backward equation

$$u_t = \frac{\epsilon a^{ij}}{2} u_{ij} + (b^i + \epsilon c^i) u_i. \quad (3.4)$$

In (3.4), subscripts indicate partial differential and repeated indices are summed from 1 to n . The coefficients a^{ij} , c^i are

$$a^{ij} = \sigma_k^i(x) \sigma_l^j(x) \left[\gamma^{kl} + \gamma^{lk} \right] \quad (3.5)$$

$$c^i = \gamma^{kl} \sigma_k^j(x) \frac{\partial}{\partial x^i} \sigma_l^i(x) \quad (3.6)$$

In practice $a(x)$ and $c(x)$ cannot be calculated from first principles, but some prescription must be given for their calculation (e.g., (10)).

Let N be a neighborhood of a stable steady state or, more generally, a domain in R^n . We set

$$\left. \begin{aligned} u(x, t) &= 1 & x \in N \\ u(x, t) &\rightarrow 0 & \text{as distance from } x \text{ to } N \rightarrow \infty \\ u(x, 0) &= \begin{cases} 0 & x \notin N \\ 1 & x \in N \end{cases} \end{aligned} \right\} \quad (3.7)$$

Then, $u(x, t)$ is the probability that $\tilde{x}(t)$ has entered N by time t , given that $\tilde{x}(0) = x$.

For stochastic relaxation theory, we are interested in the expected time to enter N , given $\tilde{x}(0) = x$ and that the process enters N :

$$T(x) = \int_0^{\infty} t u_t(x, t) dt. \quad (3.8)$$

Then $T(x)$ satisfies

$$\frac{\epsilon a^{ij}}{2} T_{ij} + (b^i + \epsilon c^i) T_i = -\bar{u}(x) \quad (3.9)$$

where

$$\bar{u}(x) = \lim_{t \rightarrow \infty} u(x, t) \quad (3.10)$$

Namely, $\bar{u}(x)$ is the probability that the process eventually enters N , given that $\tilde{x}(0) = x$. The boundary conditions appropriate to (3.9) are

$$T(x) = 0 \quad x \in N \quad (3.11)$$

and a growth condition as distance $(x, N) \rightarrow \infty$

3.2 EXACT SOLUTION AND CANONICAL FORMS

When $x \in R^1$, equation (3.9) is an ordinary differential equation

$$\frac{\varepsilon a}{2} T_{xx} + (b(x) + \varepsilon(c))T_x = -\bar{u}(x) \quad (3.12)$$

Let $N = \{x\}$. Then the solution of (3.12) is

$$T(x) = \int_x^{\Lambda} \frac{a}{\varepsilon} \exp \left[-\frac{2}{\varepsilon} \int^s \frac{b+\varepsilon c}{a} dy \right] \int_{-\infty}^s \bar{u}(x) \exp \left[\frac{2}{\varepsilon} \int^x \frac{b+\varepsilon c}{a} dy \right] dx' ds \quad (3.13)$$

Equation (3.13) has a rather complicated asymptotic analysis. Instead of doing an asymptotic analysis on (3.13), we return to (3.12) and set, for convenience $a \equiv 2$, $\bar{u}(x) \equiv 1$, and $c=0$. We will analyze (3.12) and obtain certain special functions. These functions will be generalized in section 4, for the solution of multi-dimensional problems. Our analysis is based on matched asymptotic expansions (e.g., (11)).

Away from the zeros of $b(x)$, (3.12) becomes

$$b(x)T_x = -1 \quad (3.14)$$

This is the "outer" equation.

Near zeros of $b(x)$, (3.14) breaks down. We need to stretch coordinates (3.12) to obtain the appropriate "inner" equations. We shall analyze (3.12) by using the canonical form of $b(x)$.

A. Normal Case

In the normal case, $b(x) = \pm x$, with (+) indicating that the origin is an unstable steady state, (-) indicating a stable steady state. Introducing $z = x/\sqrt{\epsilon}$, (3.12) becomes

$$T_{zz} \pm zT_z = -1 \quad (3.15)$$

B. Marginal Case

In the marginal case, the canonical dynamics are $b(x) = \pm(x^2 - \tilde{\alpha})$. We introduce the stretched variables

$z = x/\epsilon^{1/3}$, $\alpha = \tilde{\alpha}/\epsilon^{2/3}$, so that (3.12) becomes

$$T_{zz} \pm (z^2 - \alpha)T_z = -1/\epsilon^{1/3} \quad (3.16)$$

C. Critical Case

In the critical case, the canonical dynamics are $b(x) = \pm x^3 + \tilde{\beta}_1 x + \tilde{\beta}_2$. We introduce stretched variables $z = x/\epsilon^{1/4}$, $\beta_1 = \tilde{\beta}_1/\epsilon^{1/2}$, $\beta_2 = \tilde{\beta}_2/\epsilon^{3/4}$ and obtain the inner equation

$$T_{zz} + (\pm z^3 + \beta_1 z + \beta_2)T_z = -1/\epsilon^{1/2} \quad (3.17)$$

D. Hopf Case

In the Hopf case, the canonical dynamics are $b(x) = -x^3 + \tilde{\beta}x$. We introduce the stretched variables $z = x/\epsilon^{1/4}$, $\beta = \tilde{\beta}/\epsilon^{1/2}$ and obtain the inner equation

$$T_{zz} + (-z^3 + \beta z)T_z = -1/\epsilon^{1/2} \quad (3.18)$$

Equations (3.15-3.18) define certain incomplete special functions. These special functions will be used in the next section to construct asymptotic solutions of multi-dimensional problems.

SECTION 4

STOCHASTIC THEORY: ASYMPTOTIC RESULTS

When $x \in \mathbb{R}^n$ $n \geq 2$, equation (3.9) will usually not have exact solutions. Consequently, approximate techniques are required. The methods used here are closely related to those in (10). The basic idea is to generalize the one-dimensional inner solutions; we call the method a generalized ray method. Although the normal case does not represent a "critical" point, we include it for completeness.

4.1 NORMAL CASE

We suppose that the origin is a simple steady state (figure 5) and that it is stable. We seek a solution of (3.9) in the form

$$T(x) = g(x)F(\psi/\sqrt{\epsilon}) + h(x)\epsilon^{1/2} F'(\psi/\sqrt{\epsilon}) + k(x). \quad (4.1)$$

In equation (4.1), $F(z)$ is a special function satisfying

$$\frac{d^2 F}{dz^2} = z \frac{dF}{dz} - 1 \quad (4.2)$$

and the functions $\psi(x)$, $g(x)$, $h(x)$, and $k(x)$ are to be determined. In order to completely analyze the problem, we assume that g , h , k have expansions

$$g(x) = \sum g^n(x) \epsilon^n \quad h(x) = \sum h^n(x) \epsilon^n \quad k(x) = \sum k^n(x) \epsilon^n \quad (4.3)$$

Consequently, the construction given here represents the first term in the asymptotic solution of (3.9).

When derivatives are evaluated, (4.2) is used to replace $F''(\psi/\sqrt{\epsilon})$ by $\psi/\sqrt{\epsilon} F'(\psi/\sqrt{\epsilon}) - 1$. Then terms are collected according to powers of ϵ . We obtain:

$$\begin{aligned}
-\bar{u}(x) = & \epsilon^{-\frac{1}{2}} \left[b^i \psi_i + \frac{a^{ij}}{2} \psi_i \psi_j \psi \right] (g+h\psi)F' \\
& + \epsilon^0 F(b^i g_i) \\
& + \epsilon^0 (b^i k_i + \frac{a^{ij}}{2} \psi_i \psi_j g) \\
& + \epsilon^{\frac{1}{2}} F' \left[b^i h_i + \frac{a^{ij}}{2} g \psi_j + a^{ij} h_i \psi_j \psi \right. \\
& + \frac{a^{ij}}{2} h \psi_i \psi_j + \frac{a^{ij}}{2} \psi_i \psi_j h - g c^i \psi_i \\
& \left. + h c^i \psi_i \psi \right]
\end{aligned} \tag{4.4}$$

The leading terms vanish if

$$b^i \psi_i + \frac{a^{ij}}{2} \psi_i \psi_j \psi = 0 \tag{4.5}$$

$$b^i g_i = 0 \tag{4.6}$$

$$b^i k_i + \frac{a^{ij}}{2} \psi_i \psi_j g = -\bar{u}(x) \tag{4.7}$$

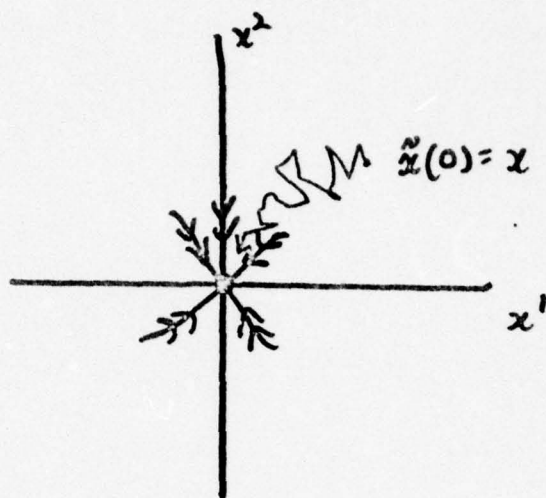
First consider (4.5). Since $b^i(0) = 0$ for all i , we set $\psi(0) = 0$, in order to keep $\psi(x)$ regular. Then (4.5) can be solved by the method of characteristics. We note that the transformation

$\phi = \frac{1}{2} \psi^2$ converts (4.5) to

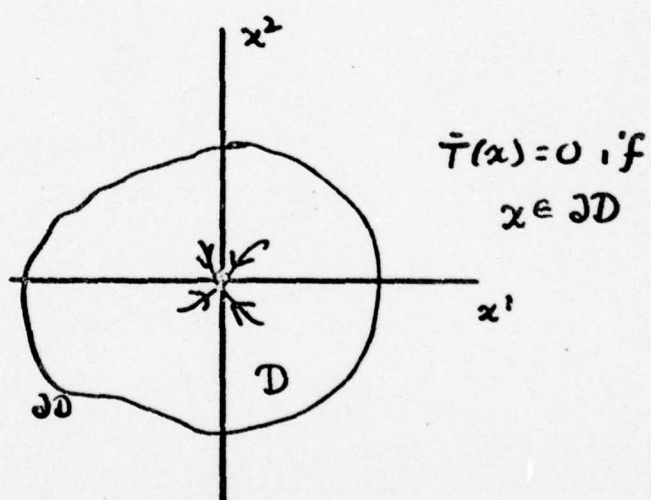
$$b^i \phi_i + \frac{a^{ij}}{2} \phi_i \phi_j = 0, \tag{4.8}$$

which is a Hamilton-Jacobi equation (see also (12)). Then, we can solve the Hamilton-Jacobi equation in terms of characteristics:

$$\dot{x}^i = \frac{\partial H}{\partial p_i} \quad \dot{p}^i = -\frac{\partial H}{\partial x^i} \quad \dot{\phi} = \frac{1}{2} a^{ij} p_i p_j \tag{4.9}$$



(a)



(b)

FIG. 5: STOCHASTIC RELAXATION PROBLEMS IN THE NORMAL CASE.
 (a) THE RELAXATION PROBLEM
 (b) THE FIRST EXIT PROBLEM

where

$$H(x, p) = b^i p_i + \frac{a^{ij}}{2} p_i p_j \quad (4.10)$$

Starting at the origin, the phase plane is covered with trajectories, called rays, along which ψ (or ϕ) is known. Thus, ψ at any point x is known.

Equation (4.3) indicates that g is constant on deterministic trajectories. Since all trajectories intersect at the origin, g must have the same value on all trajectories. At the origin, (4.7) becomes

$$\frac{a^{ij}}{2} \psi_i \psi_j g = -\bar{u}(0) = -1 \quad (4.11)$$

Thus

$$g = \frac{-1}{\frac{a^{ij}}{2} \psi_i \psi_j} \quad (4.12)$$

We set $k(0) = 0$ as initial data for (4.7).

If we set $F(0) = F'(0) = 0$ as initial conditions in (4.2), then the leading term of the asymptotic solution satisfies $T(0) \equiv 0$.

The $O(\epsilon^{1/2} F')$ term in (4.4) vanishes if

$$\begin{aligned} b^i h_i + \frac{a^{ij}}{2} g \psi_{ij} + a^{ij} h_i \psi_j \psi + \frac{a^{ij}}{2} h \psi_{ij} \psi \\ + \frac{a^{ij}}{2} \psi_i \psi_j h - g c^i \psi_i + h c^i \psi_i \psi = 0 \end{aligned} \quad (4.13)$$

At the origin $b'(0) = \psi(0) = 0$, so that (4.13) becomes

$$h(0) = \frac{1}{\frac{a_{ij}}{2} \psi_i \psi_j} \left\{ \frac{-a_{ij}}{2} \psi_{ij} g + c^i \psi_i g \right\} \quad (4.14)$$

Equation (4.13) can be solved by the method of characteristics, with initial data given by (4.14).

Thus, we have completely constructed the leading term of the asymptotic solution of (3.9).

As a by-product of our method, we are able to approximately solve the famous Kolmogorov first exit problem, recently considered by Matkowsky and Schuss (13) using matched asymptotic expansions. This problem is the following: suppose that the origin is surrounded by a domain D , with boundary ∂D . Find the expected time that the process takes to hit the boundary (i.e. the mean exit time from D) (Fig. 5b) from x .

We follow the arguments leading to equations (4.1 - 4.11), except that the initial data for F, F' and $k(x)$ change. We set $k(x) \equiv 0$ on ∂D . We distinguish two cases:

i) The boundary ∂D is a contour of ψ (or Φ) say, $\psi = \psi_D$ on ∂D . Then we set

$$F(\psi_D/\sqrt{\epsilon}) = F'(\psi_D/\sqrt{\epsilon}) = 0 \quad (4.15)$$

when solving (4.2). Then $T \equiv 0$ on D .

ii) The boundary ∂D is not a contour of ψ . Let ψ_I and ψ_{II} denote the maximum and minimum values of ψ on ∂D . Then $T \neq 0$ on ∂D , but it can be shown that on ∂D

$$|T| \leq |\ln(\psi_I/\psi_{II})| \quad (4.16)$$

+ exponentially small terms.

Hence, if $|\ln(\psi_I/\psi_{II})|$ is small, then $|T(x)|$ will be small on the boundary.

4.2 MARGINAL CASE

In some senses, the marginal case has the least interesting dynamics. The dynamical problem we consider here is sketched on figure 6. When the deterministic system has two nodes (Q_0, Q_1) and one saddle (S) , even if the process starts near Q_0 , it will eventually reach Q_1 , due to the proximity of Q_0 and S . The proper question in the stochastic theory involves the time to cross some given curve R . We note that such a time is infinite in the deterministic case, if the phase point starts on or above S .

We seek a solution of (3.9) of the form

$$T(x) = g(x)B(\psi/\epsilon^{1/3}, \beta/\epsilon^{2/3}, 1/\epsilon^{1/3}, \gamma_2) \\ + h(x)\epsilon^{2/3}B'(\beta/\epsilon^{2/3}, 1/\epsilon^{1/3}, \gamma_2) + k(x) \quad (4.17)$$

In (4.17), $B(z, \alpha, \lambda_1, \lambda_2)$ satisfies

$$\frac{d^2 B}{dz^2} = -(z^2 - \alpha) \frac{dB}{dz} - \lambda_1 + \lambda_2 z \quad (4.18)$$

and $g(x)$, $h(x)$, $k(x)$, $\psi(x)$ and the parameters α, γ_2 are to be determined. We proceed as in Section 4.1. Instead of equations (4.5-7) we obtain

$$b^i \psi_i - \frac{a^{ij}}{2} \psi_i \psi_j (\psi^2 - \beta_0) = 0 \quad (4.19)$$

$$b^i g_i = 0 \quad (4.20)$$

$$b^i k_i - \frac{a^{ij}}{2} \psi_i \psi_j g(1 + \gamma_2 \psi) = -\bar{u}(x) \quad (4.21)$$

In (4.17), we have set $\beta = \sum \beta_k \epsilon^k$.

We set $\psi^2 = \beta_0$ at Q_0 and at S . In particular $\psi(Q_0) = +\sqrt{\beta_0}$ and $\psi(S) = -\sqrt{\beta_0}$. The value of β_0 can be determined by an iterative procedure (10). We pick an initial value of $\beta_0 = \beta_0^{(0)}$ and solve (4.19) by the method of characteristics, starting at Q_0 , where $\psi = \sqrt{\beta_0^{(0)}}$. Some rays will approach S . As a ray approaches S , ψ should approach $-\sqrt{\beta_0^{(0)}}$. If it does not, then the $\beta_0^{(0)}$ must be replaced by a second iterate $\beta_0^{(1)}$. The method of false position

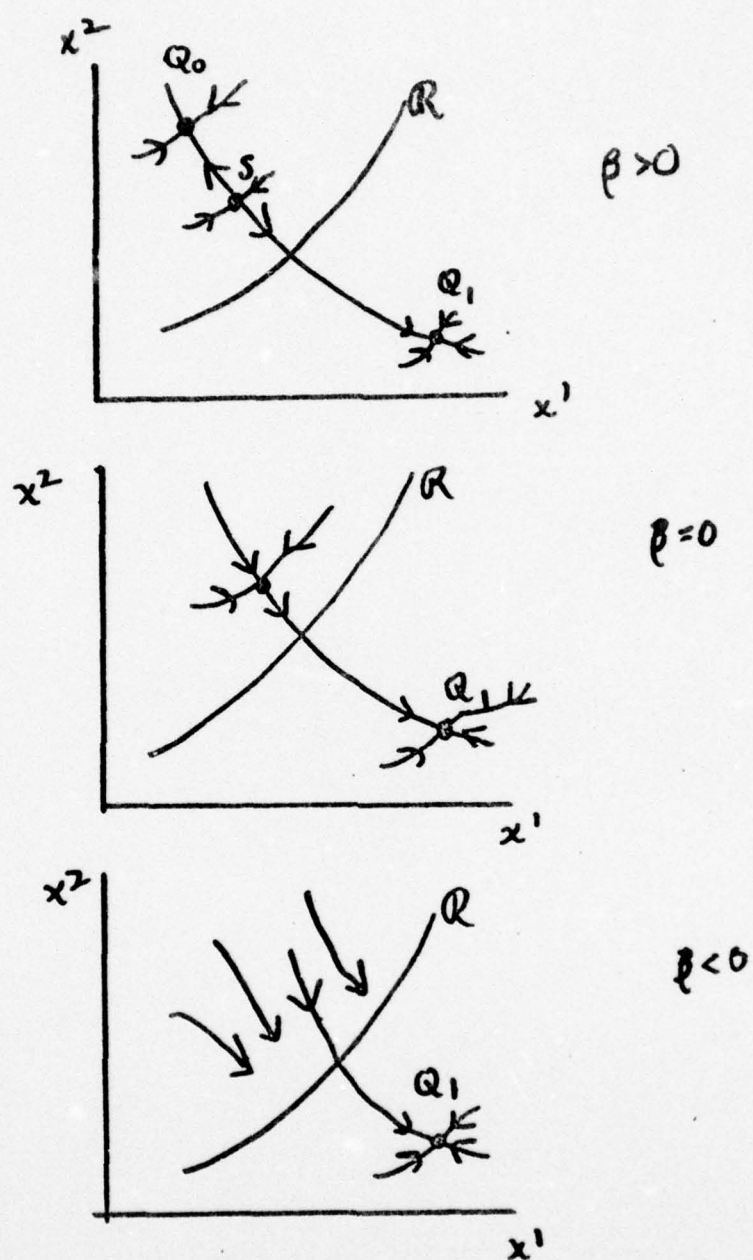


FIG. 6: RELAXATION PROBLEMS IN THE MARGINAL CASE

can be used to calculate iterates of β_0 . This procedure can be repeated until β_0 is known to any desired accuracy. (In (10), we present a discussion of this calculation in more detail.)

Equation (4.20) indicates that g is a constant. At Q_0 and Q_1 , which we denote generically by P , we have, from (4.21):

$$-\frac{a_{ij}}{2} \psi_i \psi_j \Big|_P g(1 + \gamma_2 \psi(P)) = -\bar{u}(P) \quad (4.23)$$

These are two equations for the unknowns g and γ_2 . We set $k = 0$ on R and assume that R is a level curve of ψ , with $\psi = \psi_R$ on R . Then we set

$$B(\psi_R/\epsilon^{1/3}, \beta, 1/\epsilon^{1/3}, \gamma_2) = B^1(\psi_R/\epsilon^{1/3}, \beta, 1/\epsilon^{1/3}, \gamma_2) = 0 \quad (4.21)$$

With these choices, $T(x) \equiv 0$ if $x \in R$.

At the bifurcation point $\eta = 0$ (the marginal bifurcation) Q_0 and Q_1 coalesce. Then $\beta_0 \equiv 0$, and it can be shown that $\gamma_2 \equiv 0$ (10). At the saddle-node Q_0/Q_1 , equation (4.23) still provides one equation for g :

$$g = \frac{\bar{u}(P)}{\frac{a_{ij}}{2} \psi_i \psi_j} \quad (4.24)$$

Elsewhere, we have given proofs that all the construction are regular at the bifurcation point ((10), appendices D, E).

In section 5, we consider an example of a chemical system exhibiting the marginal bifurcation.

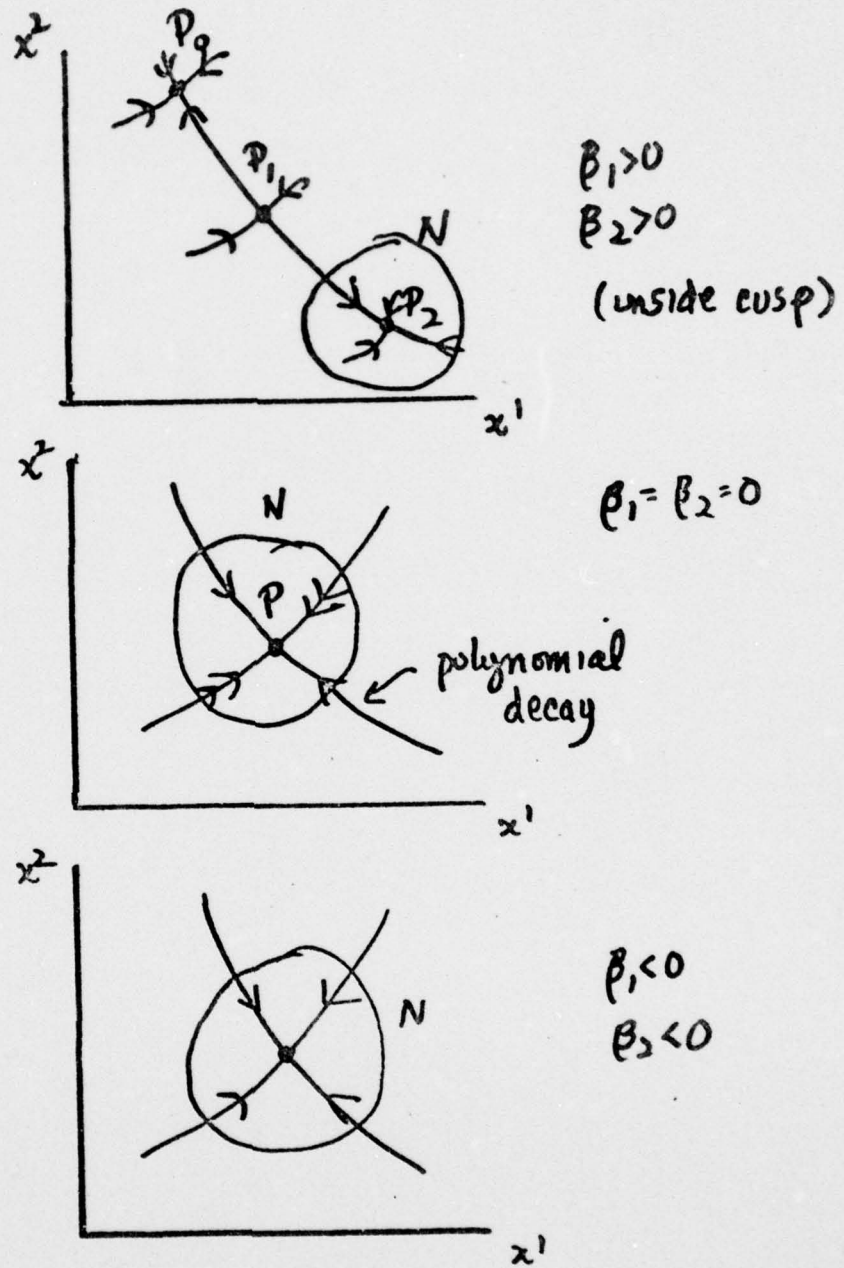


FIG. 7: RELAXATION PROBLEMS IN THE CRITICAL CASE.

4.3 CRITICAL CASE

We now consider a system with three steady states, P_0 , P_1 , and P_2 when $\alpha_1, \alpha_2 > 0$. When $\alpha_1 = \alpha_2 = 0$ the three steady states coalesce into a critical type steady state. When $\alpha_1, \alpha_2 < 0$ there is only one real steady state; it is assumed to be stable. If

$\alpha_1, \alpha_2 > 0$, we surround P_2 by a domain N and pose the following stochastic relaxation problem: what is the expected time to enter N , given the initial position. Clearly there is an analogous problem for a neighborhood N of P_0 . When there is only one steady state P , we surround P by N . We note that if N shrinks to P , then we have the expected time to "reach" P , conditioned on initial position. We also note that $T(x) \equiv 0$ if $x \in N$.

We seek a solution of (3.9) in the form

$$\begin{aligned} T(x) = & g(x) Q(\psi/\epsilon^{1/4}, \alpha/\epsilon^{1/2}, \beta/\epsilon^{3/4}, 1/\epsilon^{1/2}, \gamma_1/\epsilon^{1/4}, \gamma_2) \\ & + h(x) \epsilon^{3/4} Q(\psi/\epsilon^{1/4}, \alpha/\epsilon^{1/2}, \beta/\epsilon^{3/4}, 1/\epsilon^{1/2}, \gamma_1/\epsilon^{1/4}, \psi_2) \\ & + k(x) \end{aligned} \quad (4.25)$$

where $Q(z, \alpha, \beta, \gamma_1, \gamma_2, \gamma_3)$ satisfies

$$\frac{d^2 Q}{dz^2} = \pm (z^3 - \alpha z - \beta) \frac{dQ}{dz} - \gamma_1 + \gamma_2 z + \gamma_3 z^2 \quad (4.26)$$

The (+) sign in (4.26) corresponds to the steady state P being stable, the (-) sign to it being unstable. We consider the case in which P is stable.

Instead of (4.5), we obtain

$$b^i \psi_i + \frac{a^{ij}}{2} \psi_i \psi_j (\psi^3 - \alpha \psi - \beta) = 0. \quad (4.27)$$

When there are three steady states, α and β are determined by a procedure analogous to the one in section 4.2. Namely, at the steady states we set

$$\psi^3 - \alpha\psi - \beta = 0. \quad (4.28)$$

The method of characteristics is then used to determine α and β by an iterative procedure. When the three steady states coalesce $\alpha = \beta = 0$. When there is one real and two imaginary steady states, then $\alpha, \beta < 0$ and can be determined by power series. Such series are constructed elsewhere (10).

Instead of (4.7), we obtain

$$b^i k_i + \frac{a^{ij}}{2} \psi_i \psi_j g(-1 + \gamma_2 \psi + \gamma_3 \psi^2) = -\bar{u}(x) \quad (4.29)$$

At the steady states, we obtain

$$\frac{a^{ij}}{2} \psi_i \psi_j g(-1 + \gamma_2 \psi + \gamma_3 \psi^2) = -\bar{u}(x) \quad (4.30)$$

When there are three real steady states, we obtain three equations for g , γ_2 , and γ_3 . When two steady states coalesce, $\gamma_3 = 0$. We still have two equations for g and γ_2 . Finally, when all three coalesce, $\gamma_2 = \gamma_3 = 0$ and we are left with one equation for g .

We obtain an equation for $h(x)$ that is analogous to (4.13), and is treated in an analogous fashion. The initial values of Q and Q' in (4.26) are determined so that $T(x) \equiv 0$ if $x \in \partial N$.

4.4 HOPF CASE

The Hopf type dynamical system is treated in an identical fashion to the marginal and critical type systems. We seek a solution of (3.9) in the form

$$\begin{aligned} T(x) = & g(x)H(\psi/\epsilon^{1/4}, \beta/\epsilon^{1/2}, 1/\epsilon^{1/2}, \gamma_2/\epsilon^{1/4}) \\ & + \frac{1}{4}H'(\psi/\epsilon^{1/4}, 1/\epsilon^{1/2}, \beta/\epsilon^{1/2}, \gamma_2/\epsilon^{1/4})h(x) \\ & + k(x) \end{aligned} \quad (4.31)$$

where $H(z, \beta, \gamma_1, \gamma_2)$ satisfies

$$\frac{d^2 H}{dt^2} = \pm (z^3 - \beta z) \frac{dH}{dz} - \gamma_1 + \gamma_2 z \quad (4.32)$$

The (+) sign corresponds to a stable limit cycle and unstable focus, the (-) sign corresponds to an unstable limit cycle and stable focus. The analysis proceeds exactly as in section 4.2,3.

SECTION 5

SUBSTRATE INHIBITED REACTIONS: A MARGINAL TYPE STEADY STATE

The following equations model a substrate inhibited chemical reaction in an open reactor (10,14):

$$\dot{x}^1 = \frac{-1.4x^1}{1.5+x^1+13(x^1)^2} - .069979 x^1 + .25901 - \frac{x^1 x^2}{1+10x^1 x^2} \quad (5.1)$$

$$\dot{x}^2 = .09 - \frac{x^1 x^2}{1+10x^1 x^2} \quad (5.2)$$

where x^1 and x^2 are dimensionless "concentration" variables. The steady state (.4359, 2.065) is a saddle node, it is a marginal type steady state. The steady state (1.46, .52) is a stable node. The phase portrait is shown in figure 8, along with a first exit boundary. The theory on section 4.2 applies. We wish to calculate the expected time to hit R, conditioned on initial position. Using the birth and death approach to chemical kinetics (15), ϵa can be modeled as (10):

$$\epsilon a = \begin{pmatrix} (\lambda_1 + \mu_1)x^1 & \frac{x^1 x^2}{1+10x^1 x^2} \\ \frac{x^1 x^2}{1+10x^1 x^2} & (\lambda_2 + \mu_2)x^2 \end{pmatrix} \quad (5.3)$$

where

$$(\lambda_1 + \mu_1)x^1 = \frac{1.4x^1}{1.5+x^1+13(x^1)^2} + .069979x^1 + .25901 + \frac{x^1 x^2}{1+10x^1 x^2} \quad (5.4)$$

$$(\lambda_2 + \mu_2)x^2 = .09 + \frac{x^1 x^2}{1+10x^1 x^2} \quad (5.5)$$

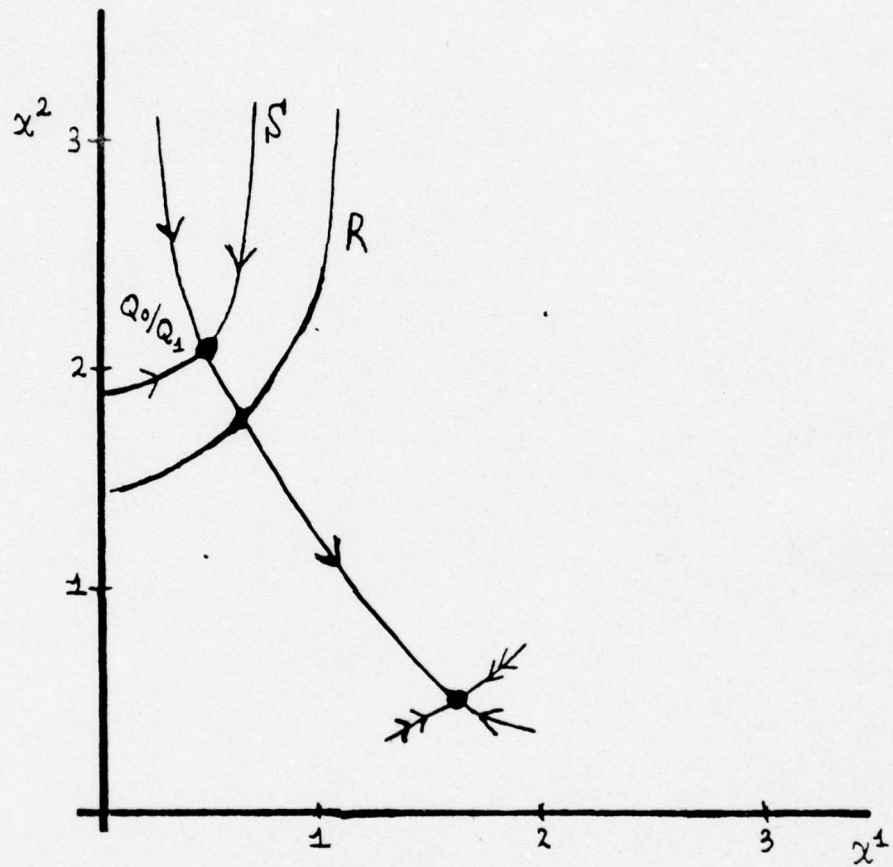


FIGURE 8: DETERMINISTIC PHASE PORTRAIT AT THE MARGINAL BIFURCATION. THE BOUNDARY R WAS USED IN THE CALCULATION OF THE MEAN EXIT TIME.

The parameter ε characterizes the intensity of fluctuation.

In table I, we compare the theory of section 4 with Monte Carlo experiments for $\varepsilon = .01$.

TABLE 1

Comparison of the Theory and Monte Carlo Experiments
in the Marginal Bifurcation

<u>Test Point</u>	<u>T(x) Theory</u>	<u>T(x) Experiment (# Trials)</u>
(.42, 2.06)	60.3	56.4 (950)
(.38, 2.36)	104.1	91.2 (400)
(.20, 2.0)	66.1	62.4 (2000)
(.3, 1.8)	37.7	35.0 (1550)
(.16, 2.4)	119.6	103.5 (400)
(.7, 2.2)	36.1	31.4 (1750)
(.6, 2.4)	74.9	68.2 (800)

SECTION 6

KINETIC MODEL OF THE FERROMAGNET

We shall give an analysis of the mean field ferromagnet, similar to that of Griffiths et. al. (2). The problem is one dimensional, so that the full theory of section 4 is not needed. However, this application illustrates many of the ideas that run through an analysis.

Consider N spins, with $\sigma_i = \pm 1$, in a magnetic field H . Let J be a coupling constant. The Hamiltonian is

$$\tilde{H} = -\frac{J}{N} \sum_{1 \leq i < j} \sigma_i \sigma_j - \mu H \sum \sigma_i - 1/2J \quad (6.1)$$

We let

$$n = \frac{1}{2} (N + \sum \sigma_i) , \quad (6.2)$$

denote the number of spins "pointing up." Then (6.1) becomes

$$\tilde{H} \equiv \phi(n) = \frac{-J(2n - N)^2}{2N} - \mu H(2n - N) \quad (6.3)$$

We take a mean field approach and assume that the number of spins pointing up is really a statistical variable, $\tilde{n}(t)$. The statistical behavior of $\tilde{n}(t)$ is described by transition probabilities:

$$\begin{aligned} & \text{Pr} \left\{ \tilde{n}(\tau + \delta\tau) - \tilde{n}(\tau) = 1 \mid \tilde{n}(\tau) = n \right\} \\ &= \frac{N - n}{N} \exp \left[\frac{-\beta}{2} \left(\phi(n + 1) - \phi(n) \right) \right] \delta\tau + o(\delta\tau) \end{aligned} \quad (6.4)$$

$$\Pr \left\{ \tilde{n}(\tau + \delta\tau) - \tilde{n}(\tau) = -1 \mid \tilde{n}(\tau) = n \right\} \quad (6.5)$$

$$= \frac{n}{N} \exp \left[\frac{-\beta}{2} (\phi(n-1) - \phi(n)) \right] \delta\tau + o(\delta\tau),$$

where $\beta = 1/k_B T$. We assume that the probability of all other transitions is $o(\delta\tau)$. In deriving (6.4,5), we have restated the argument in (2). We follow (2) and introduce a "continuous" variable

$$\tilde{x}(t) = \frac{\sum \sigma_i}{N} = \frac{2\tilde{n} - N}{N} \quad (6.6)$$

If $\delta\tilde{x} = \tilde{x}(\tau + \delta\tau) - \tilde{x}(\tau)$, then (6.4,5) become

$$\Pr \left\{ \delta\tilde{x} = 2/N \mid \tilde{x}(\tau) = x \right\} = \frac{1-x}{2} \exp \left\{ -\beta(-xJ - \frac{J}{N} - H\mu) \right\} \delta\tau + o(\delta\tau) \quad (6.7)$$

$$\Pr \left\{ \delta\tilde{x} = -2/N \mid \tilde{x}(\tau) = x \right\} = \frac{1+x}{2} \exp \left\{ -\beta(xJ - \frac{J}{N} + H\mu) \right\} \delta\tau + o(\delta\tau) \quad (6.8)$$

We set $\alpha = J\beta$, $\delta = \beta\mu H$ and introduce a macroscopic "physical" time defined by

$$t \equiv \frac{\tau}{N} \quad (6.9)$$

Thus, we construct drift and diffusion coefficients

$$b(x) = \lim_{\delta t \rightarrow 0} \frac{1}{\delta t} E \left\{ \delta\tilde{x} \mid \tilde{x}(t) = x \right\} \quad (6.10)$$

$$= (1-x) \exp \left[\alpha x + \frac{\alpha}{N} + \delta \right] - (1+x) \exp \left[-\alpha x + \frac{\alpha}{N} - \delta \right] \quad (6.11)$$

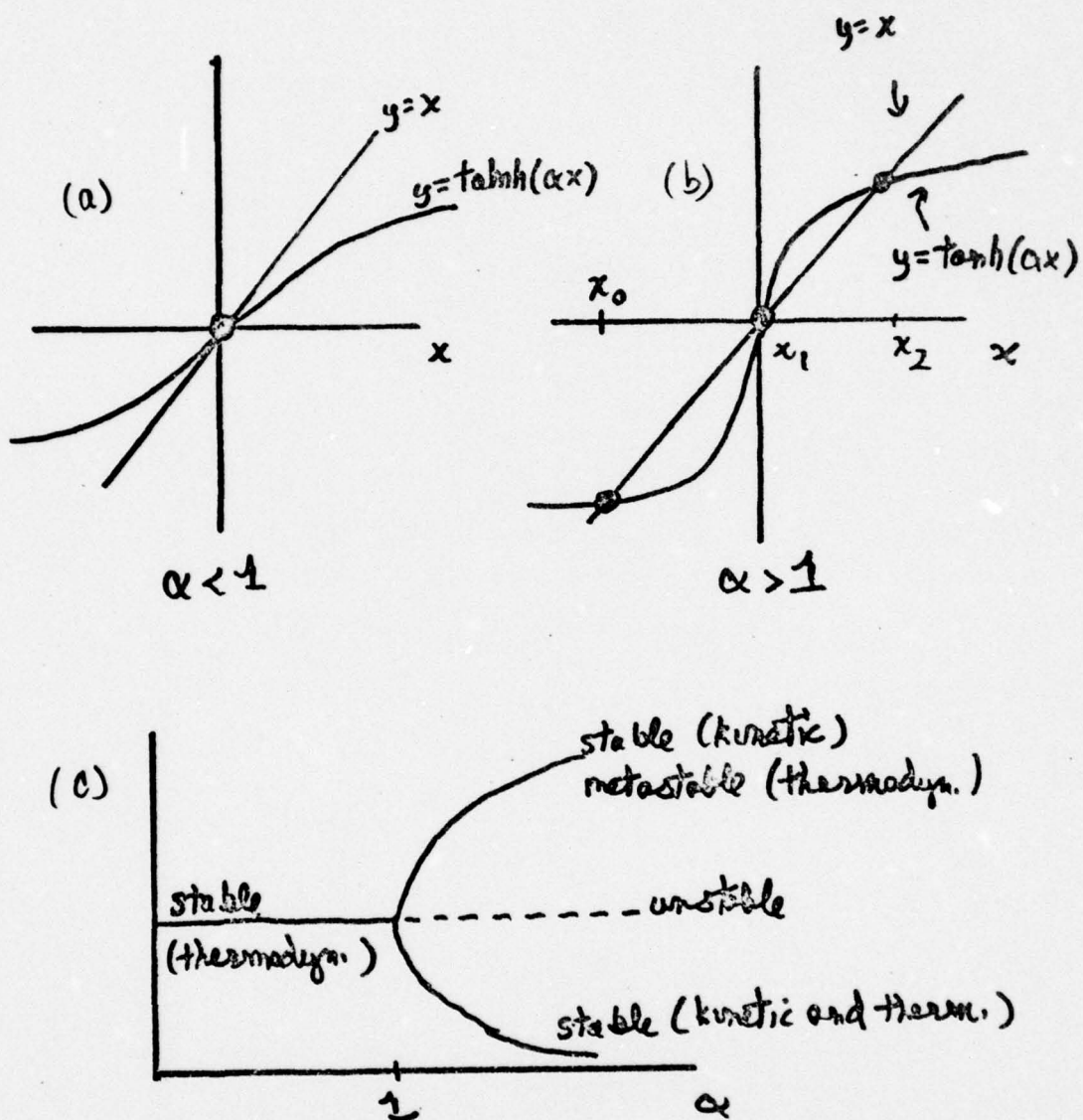


FIGURE 9: MEAN FIELD FERROMAGNET

and

$$a(x) = \lim_{\delta t \rightarrow 0} \frac{1}{\delta t} E \left\{ (\delta \tilde{x})^2 | \tilde{x}(t) = x \right\} \quad (6.12)$$

$$= \frac{1}{N} \left\{ (1 - x) \exp \left(\alpha x + \frac{\alpha}{N} + \delta \right) + (1 + x) \exp \left(-\alpha x + \frac{\alpha}{N} - \delta \right) \right\} \quad (6.13)$$

Thus, the average value of $\tilde{x}(t)$ evolves according to

$$\dot{x} = b(x, \alpha, \delta) = 2e^{\alpha/N} \left\{ \sinh(\alpha x + \delta) - x \cosh(\alpha x + \delta) \right\}, \quad (6.14)$$

subject to $-1 \leq x \leq 1$. The steady states and true (physical) equilibrium are solutions of $b(x, \alpha, \delta) = 0$. Therefore, one obtains

$$x = \tanh(\alpha x + \delta) \quad (6.15)$$

Equation (6.15) is usually obtained by a statistical thermodynamics argument (e.g. (16), pg. 101).

This agreement adds support to our statistical approach. In many respects, the approach used here is preferable to the standard approach. Not only does the stochastic approach yield the equilibrium solution, it gives dynamics and the steady states. As is well known, equation (6.15) may have 1, 2, or 3 solutions, depending upon the values of α and δ . In figures 9a, b, we illustrate the graphical solution of (6.15) for zero field ($\delta = 0$). When $\delta = 0$, x_0 and x_2 are both thermodynamically, and kinetically, stable. However, for $\delta \neq 0$, one of x_0, x_2 becomes kinetically stable

(thermodynamically metastable) while the other is the true thermodynamic (and kinetic) equilibrium (Figure 9c). The kinetic condition of criticality is that, when $\delta = 0$

$$b'(x_1) = b''(x_1) = 0 \quad (6.16)$$

We easily obtain $\alpha = 1$ as the critical value of α . This defines the critical temperature.

Now consider $\delta \neq 0$, with x_0 metastable and x_2 stable. The expected time to reach x_2 , given that $\tilde{x}(0) = x$ satisfies

$$-1 = \frac{a}{2} T_{xx} + b T_x \quad (6.17)$$

$$T(x_2) = 0 \quad \lim_{x \rightarrow -\infty} T(x) < \infty \quad (6.18)$$

with $a(x)$ and $b(x)$ given by (6.13) and (6.11). Define the relaxation rate from the metastable to stable state by

$$k = \frac{1}{T(x_0)} \quad (6.19)$$

We can calculate the relaxation rate k for all values of N . The method of Griffiths et.al. (2) broke down for large N . The result given here will be valid for all values of N . Our result thus extends their analysis. It can be shown that the two results are equivalent for small N .

SECTION 7

RELAXATION OF A CRITICAL HARMONIC OSCILLATOR

The application in section 6 did not use the theory of section 4, but the one in this section does. We consider a Duffing oscillator

$$\frac{dx}{dt} = v \quad (7.1)$$

$$m \frac{dv}{dt} = (-k(\eta)x - \alpha(x^3) - \gamma v) + \sqrt{\epsilon a} \frac{d\tilde{y}}{dt} \quad (7.2)$$

We assume that $k(\eta_c) = 0$ for some critical value of η and that $k(\eta) \geq 0$ for all η . The mean motion of the oscillator is given by

$$\dot{x} = v \quad (7.3)$$

$$\dot{v} = \frac{-kx - \alpha x^3 - \gamma v}{m} \quad (7.4)$$

When $\alpha > 0$, the origin is the only real steady state. The matrix

$$B = (b^i_{,j})|_{0,0} = \begin{pmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{\gamma}{m} \end{pmatrix} \quad (7.5)$$

has eigenvalues and eigenvectors

$$\lambda_{\pm} = \frac{-\gamma \pm \sqrt{\gamma^2 - 4k}}{2m} \quad e_{\pm} = \begin{pmatrix} 1 \\ \frac{-\gamma \pm \sqrt{\gamma^2 - 4k}}{2m} \end{pmatrix} \quad (7.6)$$

when $k \equiv 0$, the origin is a critical type steady state. According to the fluctuation dissipation theorem, for this problem

$a = 2kT\gamma\rho$, where

$$\rho = \int_0^{\infty} E(\tilde{Y}(s)\tilde{Y}(0)) ds \quad (7.7)$$

Let $T(x,v)$ be the expected time that the process takes to enter a small ellipse around the origin, given that $\tilde{X}(0) = x$, $\tilde{V}(0) = v$.

Then, for arbitrary k ,

$$-1 = \frac{kT\gamma_0}{m^2} T_{VV} + vT_x - \frac{(kx + \alpha x^3 + \gamma v)}{m} T_v \quad (7.8)$$

We introduce scaled variables by

$$\left. \begin{aligned} v &= \sqrt{\frac{E_0}{m}} v' & T &= \frac{m}{\gamma_0} T' & t &= \frac{m}{\gamma_0} t' \\ x &= \sqrt{\frac{E_0 m}{2}} x' & \gamma &= \gamma_0 \eta(x') & k &= \frac{k' \gamma_0}{\sqrt{E_0 m}} \end{aligned} \right\} \quad (7.9)$$

$$\alpha = \gamma_0 \left(\frac{\gamma_0^2}{E_0 m} \right)^{3/2} \alpha'$$

Where E_0 is some reference energy, such that $\rho kT \ll E_0$. Defining

$\epsilon = \rho kT/E_0$, we obtain (for $k(\eta) \equiv 0$)

$$-1 = \epsilon \eta T'_{v'v'} + v' T'_{x'} - (\alpha' (x')^3 + \eta' v') T'_{v'} \quad (7.10)$$

In the sequel, we drop the primes. Since the origin is a critical type steady state, the theory of section 4 applies.

The leading term in the asymptotic solution of (7.10) is

$$\begin{aligned} T(x) &\sim g^0 Q(\psi(x,v)/\epsilon^{1/4}, 0, 0, 1/\epsilon^{1/2}, 0, 0) \\ &\quad + k^0(x) + o(\epsilon^{3/4}) \end{aligned} \quad (7.11)$$

Equations (4.27) and (4.29) become

$$v\psi_x - (\alpha x^3 + \eta v)\psi_v + \eta\psi_v^2\psi^3 = 0 \quad (7.12)$$

$$vk_x^0 - (\alpha x^3 + \eta v)k_v^0 - g^0 \frac{\eta}{2} \psi_v^2 = -1 \quad (7.13)$$

In order to keep ψ regular at $(0,0)$, we set $\psi = 0$ there. In order to solve (7.12) by the method of characteristics, we need initial data for ψ_x and ψ_v . If (7.12) is differentiated with respect to v and evaluated at $(0,0)$, we obtain

$$\psi_x - \eta\psi_v = 0 \quad \text{at } (0,0) \quad (7.14)$$

When (7.12) is differentiated three times with respect to x and evaluated at $(0,0)$, we obtain

$$\psi_x^3 \psi_v^2 = \alpha/\eta \quad (7.15)$$

Thus we obtain, at $(0,0)$

$$\psi_x = (\alpha\eta)^{1/5} \quad \psi_v = \left(\alpha^{1/5}\right) \cdot \left(\eta^{4/5}\right)^{-1} \quad (7.16)$$

Higher derivatives are evaluated in a similar fashion. Thus, we can specify an ellipse around the origin:

$$N = \left\{ (x, v) : \psi(x, v) = \delta \right\} \quad (7.17)$$

We set $Q(\delta/\epsilon^{1/4}, 0, 0, 1/\epsilon^{1/2}, 0, 0) = Q'(\delta/\epsilon^{1/4}, 0, 0, 1/\epsilon^{1/2}, 0, 0) = 0$ when integrating (4.26). We also set $k(x, v) = 0$ if $(x, v) \in N$.

At the origin, (7.13) becomes

$$g^0 = \frac{2}{\eta\psi_v^2} = \frac{2}{\alpha^{2/5}} \eta^{3/5}, \quad (7.18)$$

which determines the value of g^0 . Then, on deterministic trajectories we have

$$\frac{dk^0}{dt} = -1 + \frac{g^0 \eta \psi_v^2}{2} \quad (7.19)$$

with the initial data given above. Equation (7.12) can now be solved by the method of characteristics, so that the leading term in the asymptotic solution is known.

REFERENCES

1. M. Mangel, "Uniform Treatment of Fluctuation of Critical Points", preprint (1978)
2. R.B. Griffiths, C-Y Weng and J.S. Langer, Phys. Rev. 149:301 (1966)
3. H. Haken, Rev. Mod. Phys. 47:67 (1975)
4. R. Kubo, K. Matsuo and K. Kitahara, J. Stat. Phys 9:51(1973)
5. V.I. Arnold, Russ. Math. Surveys 27:54 (1972)
6. A.N. Shoshitaishvili, Func. Anal. Appl. 6:169(1972)
7. A. Nitzan, R. Ortoleva, J. Deutch and J. Roos, J. Chem. Phys. 61:1056
8. N. Fenechel, J. Diff. Egn. 17:308 (1975)
9. G.C. Papanicolaou and W. Kohler, Comm. Pure Appl. Math 27:641 (1974)
10. M. Mangel, Technical Report 77-6, IAMS, Univ. of B.C., Vancouver, Canada (1977)
11. A. Nayfeh, "Perturbation Methods," Wiley (1973)
12. D. Ludwig, SIAM Rev. 17:605 (1975)
13. B. Matkowsky and Z. Schuss, SIAM J. Appl. Math 33:365 (1977)
14. H. Degn, Nature 217:1047
15. D. McQuarie, J. Appl. PRob 4:473 (1967)
16. C. J. Thompson, "Mathematical Statistical Mechanics," McMillan (1973)
17. B. Segre, "Some Properties of Differential Varieties and Transofrmations," Springer Verlag (1957)
18. P. Hartman, "Ordinary Differential Equations," Hartman (Baltimore) (1973)

Appendix: Classification of Two Dimensional Dynamical Systems.
The Normal Forms for Marginal and Critical Type Deterministic Systems

In this appendix, we classify planar dynamical systems into normal, marginal, or critical types. Our scheme is a generalization of the work of Kubo et.al. (4). We use Segre's method (17) to derive the local normal forms for the marginal and critical cases.

I. Normal Type Dynamical Systems

Let the dynamical system

$$\dot{x} = b(x) \quad x \in \mathbb{R}^2 \quad (A.1)$$

have a steady state at $x = x_0$. Let λ_{\pm} denote the eigenvalues of (b'_{ij}) evaluated at x_0 . The system (A.1) is of the normal type if the real parts of λ_{\pm} are non-zero. The steady state is stable if the real parts of λ_{\pm} are negative.

According to the standard theory of differential equations (18) there exists a change of variables $x \rightarrow y$ so that

$$\begin{pmatrix} \dot{y}_1 \\ \dot{y}_2 \end{pmatrix} = \begin{pmatrix} \lambda_+ & 0 \\ 0 & \lambda_- \end{pmatrix} \begin{pmatrix} y_1 \\ y_2 \end{pmatrix} + \begin{pmatrix} a_1 y_1^2 + b_1 y_1 y_2 + c_1 y_2^2 \\ a_2 y_1^2 + b_2 y_1 y_2 + c_2 y_2^2 \end{pmatrix} + O(y^3)$$

The coefficients $a_i - c_i$ are given in terms of the second derivatives of $b(x)$ evaluated at x_0 .

II. The Marginal Type Systems

The dynamical system

$$\dot{x} = b(x, \eta) \quad x \in \mathbb{R}^2 \quad \eta \in \mathbb{R} \quad (\text{A.2})$$

is assumed to have the following behavior. (A.2) is assumed to have three real steady states for $\eta > 0$. We denote these by $Q_0(\eta)$, $Q_1(\eta)$

P_2 .

Denote by B_k the matrix (b_{ij}^k) evaluated at Q_0, Q_1 , or P_2 . ($k=0,1,2$).

We assume

1) For all η, B_2 has two real negative eigenvalues

2) As $\eta \rightarrow 0$, the distance between $Q_0(\eta)$ and $Q_1(\eta)$ decreases.

When $\eta = 0$ the two points coalesce and annihilate each other

3) For $\eta > 0, B_0$ has two real, negative eigenvalues which depend upon η and B_1 has one real positive and one real negative eigenvalue. When $\eta = 0$, $B_0 = B_1$ has one zero and real negative eigenvalue. The eigenvector corresponding to the negative eigenvalue has positive slope.

We introduce as new coordinates the eigenvectors y_1, y_2 as new coordinates so that (A.2) becomes

$$\begin{aligned} \dot{y}_1 &= \mathfrak{B}^1(y, \eta) \\ \dot{y}_2 &= \mathfrak{B}^2(y, \eta) \end{aligned} \quad (\text{A.2a})$$

The system (A.2) is of the marginal type if the above conditions hold and

$$a) \quad \frac{\partial \tilde{b}^1}{\partial y_1} (0,0) = 0 \quad (A.3)$$

$$b) \quad \frac{\partial^2 \tilde{b}^1}{\partial y_1^2} (0,0) = a \neq 0.$$

When η is small, but non-zero, we translate the origin, so that the system (A.2) is approximately given by

$$\left\{ \begin{array}{l} \dot{y}_1 = \tilde{c}_1 \eta + \tilde{c}_2 \eta y_1 + a y_1^2 + \tilde{b}_{y_1} y_2 + \tilde{c}_{y_2}^2 \\ \quad \quad \quad + O(y^3, \eta^2) \\ \dot{y}_2 = \tilde{\lambda}(\eta) y_2 + O(y^2, \eta) \end{array} \right. \quad (A.4)$$

In (A.4), $\tilde{\lambda}(\eta)$ is the non-zero eigenvalue of $B(\eta) = (b'_{ij}(\eta)) | x_1$.

The coefficient a is given by A.3b; the other coefficients are also given in terms of the derivatives of $b(x)$. We assume $c_1 \neq 0$

Let $y' = \frac{1}{a} \dot{y}$. Then (A.4) becomes

$$\left\{ \begin{array}{l} y_1' = c_1 \eta + c_2 \eta y_1 + y_1^2 + b_{y_1} y_2 + c_{y_2}^2 + O(y^3, \eta^2) \\ y_2' = \lambda_0 y_2 + O(y^2, \eta) \end{array} \right. \quad (A.5)$$

where $s = \tilde{s}/a$.

Introduce new coordinates by

$$\left\{ \begin{array}{l} z_1 = y_1 + s y_1 y_2 + t y_1^2 + u y_2^2 + w y_1 \eta + r y_2 \eta \\ \quad \quad \quad + O(\eta^2, y^3, \eta y^2) \\ z_2 = y_2 + O(\eta, y^2) \end{array} \right. \quad (A.6)$$

then

$$\begin{aligned}
 z'_2 &= y'_2 = \lambda_0 z_2 + o(\eta, z^2) \\
 z'_1 &= y'_1 + sy'_1 y_2 + sy_1 y'_2 + 2ty_1 y'_1 \\
 &\quad + 2uy_2 y'_2 + wy'_1 \eta + ry'_2 \eta \\
 &\quad + o(\eta y y', y^2 y')
 \end{aligned} \tag{A.7}$$

Using (A.5) in (A.7) yields

$$\begin{aligned}
 z'_2 &= \lambda_0 z_2 + o(\eta, z^2) \\
 z'_1 &= c_1 \eta + y_1 (c_2 \eta + 2tc_1 \eta) + y_1^2 \\
 &\quad + y_1 y_2 (b + s\lambda_0) + y_2 (r\eta\lambda + sc_1 \eta) \\
 &\quad + y_2^2 (2u\lambda + c) + o(y^3, \eta y^2, \eta^2)
 \end{aligned} \tag{A.8}$$

We choose

$$\begin{aligned}
 t &= \frac{-c_2}{2c_1} & s &= \frac{-b}{\lambda_0} & r &= \frac{-sc_1}{\lambda} \\
 u &= \frac{-c}{2\lambda}
 \end{aligned}$$

and note that $y_1^2 = z_1^2 + o(y^3)$. Thus equation (A.8) becomes

$$\begin{aligned}
 z'_2 &= \lambda_0 z_2 + o(\eta, z^2) \\
 z'_1 &= z_1^2 - \beta(\eta) + o(z^3, \eta z^2, \eta^2)
 \end{aligned} \tag{A.9}$$

where $\beta(\eta) = -c_1 \eta$. Equation (A.9) is the local normal form which we desire. It is a weaker result than that of Arnol'd (5) or Shoshaitshvili (6) who actually eliminate the higher order terms.

III. Critical Type Systems

We now consider a dynamical system depending upon two parameters

$$\dot{x} = b(x, \eta, \delta) \quad x \in \mathbb{R}^2 \quad \eta, \delta \in \mathbb{R} \quad (\text{A.10})$$

We make the following assumptions:

1) For some combinations of η and δ , equation (A.10) has three steady states $P_0(\eta, \delta)$, $P_1(\eta, \delta)$ and $P_2(\eta, \delta)$. When the three points are distinct, we assume that P_0 and P_2 are stable nodes and that P_1 is a saddle point.

2) As η, δ vary, two of the points may coalesce into a point of neutral stability (i.e., one eigenvalue of the linearized equations is zero). This situation is equivalent to a marginal type dynamical system.

3) As $\eta, \delta \rightarrow 0$ from above, the three steady states approach each other and coalesce when $\eta = \delta = 0$. Let $B = (b_{ij}^i)$ evaluated at P_1 . When $\eta, \delta > 0$, we assume that B has one real positive and one real negative eigenvalue. When $\eta = \delta = 0$, B has one real negative and one zero eigenvalue. When $\eta, \delta < 0$, B has two real negative eigenvalues.

We denote by $y_1(\eta, \delta)$, $y_2(\eta, \delta)$ the eigenvectors of B .

The eigenvectors y_1, y_2 are introduced as new coordinates so that (A.10) becomes

$$\dot{y}_1 = \tilde{b}^1(y, \eta, \delta)$$

(A.10a)

$$\dot{y}_2 = \tilde{b}^2(y, \eta, \delta)$$

The system A.10a is of the critical type if

a) at $\eta = \delta = 0$, B has one zero eigenvalue

b) the second derivatives

$$\left. \frac{\partial^2 \tilde{b}}{\partial y_1^2} \right|_{(0,0,)}, \quad \frac{\partial^2 \tilde{b}}{\partial y_1 \partial y_2}, \quad \frac{\partial^2 \tilde{b}}{\partial y_2^2} \quad \text{vanish}$$

(A.11)

when $\eta = \delta = 0$

$$c) \quad \frac{\partial^2 \tilde{b}}{\partial y_1^3} = a \neq 0.$$

The assumption on A.10b can actually be weakened slightly: we only need to require that $\frac{\partial^2 \tilde{b}}{\partial y_1^2}$ vanish, the other second derivatives

need not vanish. However, assumption A.10b does not cause any loss of generality and simplifies the analysis considerably.

In terms of the y coordinates, for small η, δ the system (A.10) takes the form

$$\dot{y}_2 = \tilde{\chi}(\eta, \delta)y_2 + O(y^2, (\eta + \delta)y)$$

$$\dot{y}_1 = \tilde{c}_1\eta + \tilde{c}_2\delta + y_1(\tilde{c}_3\eta + \tilde{c}_4\delta)$$

(A.12)

$$+ y_1^2(\tilde{c}_5\eta + \tilde{c}_6\delta) + y_1y_2(\tilde{c}_7\eta + \tilde{c}_8\delta)$$

$$+ y_2^2 (\tilde{c}_9 \eta + \tilde{c}_{10} \delta) + a y_1^3 + b y_1^2 y_2$$

$$+ \tilde{c}_{y_1} y_2^2 + \tilde{d} y_2^3 + o(y^4, (\eta^2 + \delta^2) y_1$$

(A.12)
cont'd

$$(\eta + \delta) y^3)$$

Letting $y' = \frac{1}{a} \dot{y}$, $s = \tilde{s}/a$ and $\delta_i = c_{2i-1} \eta + c_{2i} \delta$ we have

$$y_2' = \lambda_0 y_2 + o(y^2, (\eta + \delta) y)$$

$$y_2' = \gamma_1 + \gamma_2 y_1 + \gamma_3 y_1^2 + \gamma_4 y_1 y_2$$

(A.13)

$$+ \gamma_5 y_2^2 + \gamma_1^3 + b y_1^2 y_2$$

$$+ c y_1 y_2^2 + d y_2^3$$

$$+ o(y^4, (\eta^2 + \delta^2) y,$$

$$(\eta + \delta) y^3)$$

We now introduce new variables by

$$z_2 = y_2 + o(y^2, (\eta + \delta) y)$$

$$z_1 = y_1 + s_1 \eta y_1^2 + t_1 \eta y_1 y_2 + u_1 \eta y_2^2$$

$$+ s_2 \delta y_1^2 + t_2 \delta y_1 y_2 + u_2 \delta y_2^2$$

(A.14)

$$+ w_1 y_1^3 + w_2 y_1^2 y_2 + w_3 y_1 y_2^2$$

$$+ w_4 y_2^3 + o(y^4, (\eta^2 + \delta^2) y, \eta y^3)$$

Without loss of generality, we have not included terms $o(y^2)$ in the definition of z_1 . This follows from assumption A.10b.

From A.14, we have

$$z_2 = y_2 + 0(y_2, (\eta + \delta)y_2)$$

$$\begin{aligned} z_1' = & y_1' + 2s_1 \eta y_1 y_1' + t_1 \eta y_1 y_2' \\ & + t_1 \eta y_1' y_2 + 2u_1 \eta y_2 y_2' + 2s_2 y_k y_k' \delta \\ & + t_2 \delta (y_1 y_2' + y_1' y_2) + 2u_2 \delta y_2 y_2' \\ & + 3w_1 y_1^2 y_1' + w_2 (y_1' y_1 y_2 + y_1^2 y_2') \\ & + w_3 (y_1' y_2^2 + 2y_1 y_2 y_2') \\ & + 3w_4 y_2^2 y_2' \\ & + 0(y^3 y', \eta^2 y', \delta^2 y') \end{aligned} \quad (A.15)$$

Using (A.13) in (A.15) yields (with $\lambda = \lambda_0$)

$$\begin{aligned} z_2' = & \lambda_0 z_2 + 0(z^2, \eta z) \\ z_1' = & y_1 + y_1 y_2 \\ & + y_1^2 (\gamma_3 + 3w_1 y_1) \\ & + y_1 y_2 (\gamma_4 + t_1 \eta \lambda + t_2 \delta \lambda + w_2 \lambda_1 + 2\lambda w_3) \\ & + y_2^2 (\gamma_5 + 2u_1 \eta \lambda + 2u_2 \delta \lambda + w_3 \lambda_1) \\ & + y_1^3 \\ & + y_1^2 (b + w_2 \lambda + w_2 \lambda + w_2 y_2) \end{aligned} \quad (A.16)$$

$$\begin{aligned}
& + y_1 y_2^2 (c + 2w_3 \lambda + w_3 \gamma_2) \\
& + y_2^3 (d + 3w_4 \lambda) \\
& + O(y^4, (\eta^2 + \delta^2) y, y^3 (\eta + \delta))
\end{aligned}$$

We choose

$$\begin{aligned}
w_4 &= \frac{-d}{3\lambda} & w_3 &= \frac{-c}{2\lambda + \gamma_2} & w_2 &= \frac{-b}{\lambda + \gamma_2} \\
u_1 \eta + u_2 \delta &= \frac{-\gamma_5 - w_3 \gamma_1}{2\lambda} \\
t_1 \eta + t_2 \delta &= \frac{-\gamma_4 - w_2 \gamma_1 - 2\lambda w_3}{\lambda} \\
w_1 &= \frac{-\gamma_3}{3\gamma_1} .
\end{aligned}$$

Noting that $y_1^3 = z_1^3 + O(\eta y^3, \eta^2 y^2)$ and

that $y_1 \gamma_1 = z_1 \gamma_1 + O(\eta^2 z^2)$, eqn (A.16)

becomes

$$\begin{aligned}
z_2' &= \lambda_0 z_2 + O(z^2, \eta z) \\
z_1' &= \gamma_1 + \gamma_2 z_1 + z_1^3 + O(z^4, (\eta^2 + \delta^2), \\
& \quad (\eta + \delta) z^3),
\end{aligned}$$

which is the desired normal form.

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**Research supported in part under Office of Naval Research Contract N00014-68-0273-0017
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*Research supported by the National Science Foundation
- PP 142
Lockman, Robert F., Jehn, Christopher, and Shughart, William F. II, "Models for Estimating Premature Losses and Recruiting District Performance," 36 pp., Dec 1975 (Presented at the RAND Conference on Defense Manpower, Feb 1976; to be published in the conference proceedings) AD A 020 443
- PP 143
Horowitz, Stanley and Sherman, Allan (LCDR., USN), "Maintenance Personnel Effectiveness in the Navy," 33 pp., Jan 1976 (Presented at the RAND Conference on Defense Manpower, Feb 1976; to be published in the conference proceedings) AD A 021 581
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Durch, William J., "The Navy of the Republic of China - History, Problems, and Prospects," 66 pp., Aug 1976 (To be published in "A Guide to Asiatic Fleets," ed. by Barry M. Blechman; Naval Institute Press) AD A 030 460
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Kelly, Anne M., "Port Visits and the "Internationalist Mission" of the Soviet Navy," 36 pp., Apr 1976 AD A 023 436
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Palmour, Vernon E., "Alternatives for Increasing Access to Scientific Journals," 6 pp., Apr 1975 (Presented at the 1975 IEEE Conference on Scientific Journals, Cherry Hill, N.C., Apr 28-30; published in IEEE Transactions on Professional Communication, Vol. PC-18, No. 3, Sep 1975) AD A 021 798
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Kessler, J. Christian, "Legal Issues in Protecting Offshore Structures," 33 pp., Jun 1976 (Prepared under task order N00014-68-A-0091-0023 for ONR) AD A 028 389
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McConnell, James M., "Military-Political Tasks of the Soviet Navy in War and Peace," 62 pp., Dec 1975 (Published in Soviet Oceans Development Study of Senate Commerce Committee October 1976) AD A 022 590
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Squires, Michael L., "Counterforce Effectiveness: A Comparison of the Tsipis "K" Measure and a Computer Simulation," 24 pp., Mar 1976 (Presented at the International Study Association Meetings, 27 Feb 1976) AD A 022 591
- PP 150
Kelly, Anne M. and Petersen, Charles, "Recent Changes in Soviet Naval Policy: Prospects for Arms Limitations in the Mediterranean and Indian Ocean," 28 pp., Apr 1976, AD A 023 723
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Horowitz, Stanley A., "The Economic Consequences of Political Philosophy," 8 pp., Apr 1976 (Reprinted from Economic Inquiry, Vol. XIV, No. 1, Mar 1976)
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Mizrahi, Maurice M., "On Path Integral Solutions of the Schrodinger Equation, Without Limiting Procedure," 10 pp., Apr 1976 (Reprinted from Journal of Mathematical Physics, Vol. 17, No. 4 (Apr 1976), 566-575).
*Research supported by the National Science Foundation
- PP 153
Mizrahi, Maurice M., "WKB Expansions by Path Integrals, With Applications to the Anharmonic Oscillator," 137 pp., May 1976, AD A 025 440
*Research supported by the National Science Foundation
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Mizrahi, Maurice M., "On the Semi-Classical Expansion in Quantum Mechanics for Arbitrary Hamiltonians," 19 pp., May 1976 (Published in Journal of Mathematical Physics, Vol. 18, No. 4, p. 786, Apr 1977), AD A 025 441
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Squires, Michael L., "Soviet Foreign Policy and Third World Nations," 26 pp., Jun 1976 (Prepared for presentation at the Midwest Political Science Association meetings, Apr 30, 1976) AD A 028 388
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Wilson, Desmond P., Jr., "The U.S. Sixth Fleet and the Conventional Defense of Europe," 50 pp., Sep 1976 (Submitted for publication in Adelphi Papers, I.I.S.S., London) AD A 030 457
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Melich, Michael E. and Peet, Vice Adm. Ray (USN, Retired), "Fleet Commanders: Afloat or Ashore?" 9 pp., Aug 1976 (Reprinted from U.S. Naval Institute Proceedings, Jun 1976) AD A 030 456
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Lockman, Robert F., "A Model for Predicting Recruit Losses," 9 pp., Sep 1976 (Presented at the 84th annual convention of the American Psychological Association, Washington, D.C., 4 Sep 1976) AD A 030 459
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Mahoney, Robert B., Jr., "An Assessment of Public and Elite Perceptions in France, The United Kingdom, and the Federal Republic of Germany, 31 pp., Feb 1977 (Presented at Conference "Perception of the U.S. - Soviet Balance and the Political Uses of Military Power" sponsored by Director, Advanced Research Projects Agency, April 1976) AD A 036 599
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Jondrow, James M., "Effects of Trade Restrictions on Imports of Steel," 67 pp., November 1976, (Delivered at ILAB Conference in Dec 1976)
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Classen, Kathleen P., "Unemployment Insurance and the Length of Unemployment," Dec 1976, (Presented at the University of Rochester Labor Workshop on 16 Nov 1976)
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Felix, Wendi, "Correlates of Retention and Promotion for USNA Graduates," 38 pp., Mar 1977, AD A039 040
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Lockman, Robert F. and Warner, John T., "Predicting Attrition: A Test of Alternative Approaches," 33 pp. Mar 1977. (Presented at the OSD/ONR Conference on Enlisted Attrition Xerox International Training Center, Leesburg, Virginia, 4-7 April 1977), AD A039 047
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Kleinman, Samuel D., "An Evaluation of Navy Unrestricted Line Officer Accession Programs," 23 pp. April 1977, (To be presented at the NATO Conference on Manpower Planning and Organization Design, Stresa, Italy, 20 June 1977), AD A039 048
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Stoloff, Peter H. and Balut, Stephen J., "Vacate: A Model for Personnel Inventory Planning Under Changing Management Policy," 14 pp. April 1977, (Presented at the NATO Conference on Manpower Planning and Organization Design, Stresa, Italy, 20 June 1977), AD A039 049
- PP 180
Horowitz, Stanley A. and Sherman, Allan, "The Characteristics of Naval Personnel and Personnel Performance," 16 pp. April 1977, (Presented at the NATO Conference on Manpower Planning and Organization Design, Stresa, Italy, 20 June 1977), AD A039 050
- PP 181
Balut, Stephen J. and Stoloff, Peter, "An Inventory Planning Model for Navy Enlisted Personnel," 35 pp., May 1977, (Prepared for presentation at the Joint National Meeting of the Operations Research Society of America and The Institute for Management Science, 9 May 1977, San Francisco, California), AD A042 221
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Murray, Russell, 2nd, "The Quest for the Perfect Study or My First 1138 Days at CNA," 57 pp., April 1977
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Kassing, David, "Changes in Soviet Naval Forces," 33 pp., November, 1976, (Published as part of Chapter 3, "General Purpose Forces: Navy and Marine Corps," in Arms, Men, and Military Budgets, Francis P. Hoerber and William Schneider, Jr. (eds.), (Crane, Russak & Company, Inc.: New York), 1977), AD A040 106
- PP 184
Lockman, Robert F., "An Overview of the OSD/ONR Conference on First Term Enlisted Attrition," 22 pp., June 1977, (Presented to the 39th MORS Working Group on Manpower and Personnel Manning, Annapolis, Md., 28-30 June 1977), AL A043 618
- PP 185
Kassing, David, "New Technology and Naval Forces in the South Atlantic," 22 pp. (This paper was the basis for a presentation made at the Institute for Foreign Policy Analyses, Cambridge, Mass., 28 April 1977), AD A043 619
- PP 186
Mizrahi, Maurice M., "Phase Space Integrals, Without Limiting Procedure," 31 pp., May 1977, (Invited paper presented at the 1977 NATO Institute on Path Integrals and Their Application in Quantum Statistical, and Solid State Physics, Antwerp, Belgium, July 17-30, 1977) (Published in Journal of Mathematical Physics 19(1), p. 298, Jan 1978), AD A040 107
- PP 187
Coile, Russell C., "Nomography for Operations Research," 35 pp., April 1977, (Presented at the Joint National Meeting of the Operations Research Society of America and The Institute for Management Services, San Francisco, California, 9 May 1977), AD A043 620
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Durch, William J., "Information Processing and Outcome Forecasting for Multilateral Negotiations: Testing One Approach," 53 pp., May 1977 (Prepared for presentation to the 18th Annual Convention of the International Studies Association, Chase-Park Plaza Hotel, St. Louis, Missouri, March 16-20, 1977), AD A042 222
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Coile, Russell C., "Error Detection in Computerized Information Retrieval Data Bases," July, 1977, 13 pp. Presented at the Sixth Cranfield International Conference on Mechanized Information Storage and Retrieval Systems, Cranfield Institute of Technology, Cranfield, Bedford, England, 26-29 July 1977, AD A043 580
- PP 190
Mahoney, Robert B., Jr., "European Perceptions and East-West Competition," 96 pp., July 1977 (Prepared for presentation at the annual meeting of the International Studies Association, St. Louis, Mo., March, 1977), AD A043 661
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Holen, Arlene, "Effects of Unemployment Insurance Entitlement on Duration and Job Search Outcome," August 1977, 6 pp., (Reprinted from Industrial and Labor Relations Review, Vol. 30, No. 4, Jul 1977)
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Horowitz, Stanley A., "A Model of Unemployment Insurance and the Work Test," August 1977, 7 pp. (Reprinted from Industrial and Labor Relations Review, Vol. 30, No. 40, Jul 1977)
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Classen, Kathleen P., "The Effects of Unemployment Insurance on the Duration of Unemployment and Subsequent Earnings," August 1977, 7 pp. (Reprinted from Industrial and Labor Relations Review, Vol. 30, No. 40, Jul 1977)
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Brechling, Frank, "Unemployment Insurance Taxes and Labor Turnover: Summary of Theoretical Findings," 12 pp. (Reprinted from Industrial and Labor Relations Review, Vol. 30, No. 40, Jul 1977)
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Ralston, J. M. and Lorimer, O. G., "Degradation of Bulk Electroluminescent Efficiency in Zn, O-Doped GaP LED's," July 1977, 3 pp. (Reprinted from IEEE Transactions on Electron Devices, Vol. ED-24, No. 7, July 1977)
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Wells, Anthony R., "The Centre for Naval Analyses," 14 pp., Dec 1977, AD A049 107
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Classen, Kathleen P., "The Distributional Effects of Unemployment Insurance," 25 pp., Sept. 1977 (Presented at a Hoover Institution Conference on Income Distribution, Oct 7-8, 1977)
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Durch, William J., "Revolution From A F.A.R. - The Cuban Armed Forces in Africa and the Middle East," Sep 1977, 16 pp., AD A046 268
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Powers, Bruce F., "The United States Navy," 40 pp. Dec 1977. (To be published as a chapter in The U.S. War Machine by Salamander Books in England during 1978), AD A049 108
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Durch, William J., "The Cuban Military in Africa and The Middle East: From Algeria to Angola," Sep 1977, 67 pp., AD A045 675
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Feldman, Paul, "Why Regulation Doesn't Work," (Reprinted from *Technological Change and Welfare in the Regulated Industries and Review of Social Economy*, Vol. XXIX, March, 1971, No. 1.) Sep 1977, 8 pp.
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Wells, Anthony R., "The 1967 June War: Soviet Naval Diplomacy and The Sixth Fleet - A Re-appraisal," Oct 1977, 36 pp., AD A047 236
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Coile, Russell C., "A Bibliometric Examination of the Square Root Theory of Scientific Publication Productivity," (Presented at the annual meeting of the American Society for Information Science, Chicago, Illinois, 29 September 1977.) Oct 1977, 6 pp., AD A047 237
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McConnell, James M., "Strategy and Missions of the Soviet Navy in the Year 2000," 48 pp., Nov 1977, (Presented at a Conference on Problems of Sea Power as we Approach the 21st Century, sponsored by the American Enterprise Institute for Public Policy Research, 6 October 1977, and subsequently published in a collection of papers by the Institute), AD A047 244
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- PP 209 - Classified.
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Kassing, David, "Protecting The Fleet," 40 pp., Dec 1977 (Prepared for the American Enterprise Institute Conference on Problems of Sea Power as We Approach the 21st Century, October 6-7, 1977), AD A049 109
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Weinland, Robert G., "A Somewhat Different View of The Optimal Naval Posture," 37 pp., Jun 1978 (Presented at the 1976 Convention of the American Political Science Association (APSA/IUS Panel on "Changing Strategic Requirements and Military Posture"), Chicago, Ill., September 2, 1976)
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Coile, Russell C., "Comments on: *Principles of Information Retrieval* by Manfred Kochen, 10 pp., Mar 78, (Published as a Letter to the Editor, *Journal of Documentation*, Vol. 31, No. 4, pages 298-301, December 1975)
- PP 216
Coile, Russell C., "Lotka's Frequency Distribution of Scientific Productivity," 18 pp., Feb 1978, (Published in the *Journal of the American Society for Information Science*, Vol. 28, No. 6, pp. 366-370, November 1977)
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Coile, Russell C., "Bibliometric Studies of Scientific Productivity," 17 pp., Mar 78, (Presented at the Annual meeting of the American Society for Information Science held in San Francisco, California, October 1976.)
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Mizrahi, Maurice M., "Correspondence Rules and Path Integrals," 30 pp., Jun 1978 (Invited paper presented at the CNRS meeting on "Mathematical Problems in Feynman's Path Integrals," Marseille, France, May 22-26, 1978)
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Mangel, Marc, "Stochastic Mechanics of Molecule-Molecule Reactions," 21 pp., Jun 1978 (To be submitted for publication in *Journal of Mathematical Physics*)
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"Portions of this work were started at the Institute of Applied Mathematics and Statistics, University of British Columbia, Vancouver, B.C., Canada
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"Portions of this work were completed at the Institute of Applied Mathematics and Statistics, University of British Columbia, Vancouver, Canada.
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